

DEGRADATION OF SELECTED ORGANIC AGROCHEMICALS IN
ARTIFICIAL SOIL SLURRY SYSTEMS BY ANODIC FENTON TREATMENT

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DEGRADATION OF SELECTED ORGANIC AGROCHEMICALS IN ARTIFICIAL SOIL SLURRY SYSTEMS BY ANODIC FENTON TREATMENT

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This thesis investigated the application of anodic Fenton treatment to the degradation of several probe agrochemicals in model soil slurry systems. A kinetic model, called the slurry AFT model, was developed to describe the degradation process in the slurry system. Effects of different model soil components, such as humic acid, kaolin or montmorillonite clay, and goethite, on the degradation of different groups of agrochemicals, including carbaryl, mecoprop, paraquat, 4,6-o-dinitrocresol, p-nitrophenol and dinoseb, were studied.

The results indicate that humic acid content is the key factor that slows down pesticide degradation, most probably due to its pH buffering and adsorption capacity. A kinetic model, which was shown to fit the experimental data quite well ($R^2 > 0.99$), was developed to describe the carbaryl degradation in the soil slurry during the AFT process. In the presence of humic acid, carbaryl degradation kinetics were found to shift to a pseudo-first order reaction after an “initiation” stage.

The adsorption and degradation behaviors of neutral (carbaryl), anionic (mecoprop) and cationic (paraquat) agrochemicals were studied in a slurry of Swy-2 Na^+ -montmorillonite clay. Results show that, due to different adsorption mechanisms, the adsorption effect on chemical degradation by anodic Fenton treatment (AFT) varies with pesticide: strong and tight adsorption of paraquat at the clay interlayer protects paraquat from being attacked by hydroxyl radicals; loosely adsorbed carbaryl or mecoprop is readily degraded. XRD analysis clearly indicates that AFT is capable of effectively degrading interlayer non-cationic organic chemicals that are not usually

available for biodegradation.

The adsorption and degradation of 4, 6-*o*-dinitroresol (DNOC) and *p*-nitrophenol (PNP) in Swy-2 montmorillonite clay slurry were investigated. The pH and type of cation were varied, and results showed that adsorption of DNOC and PNP increased at lower pH values. The specific cation had a significant effect on adsorption, which was dramatically enhanced in the presence of K^+ and NH_4^+ . It was found that the DNOC degradation rate substantially decreased in the clay slurry system in the presence of K^+ and low pH, with a large amount of DNOC residue remaining after 60 min treatment. Based on LC-MS data, a DNOC degradation pathway was proposed. Overall, the results showed the inhibition effect of specific adsorption mechanisms on the degradation of nitroaromatic compounds in montmorillonite clay slurry by AFT, providing important implications for water and soil remediation.

The pH effect on the adsorption and AFT degradation of dinoseb in a goethite slurry was investigated. At neutral or high pH, there was less dinoseb adsorption on goethite, and the AFT degradation process was not significantly affected. At an acidic or low pH, there was much more dinoseb adsorption on the goethite, and the AFT degradation process was inhibited by the adsorption, though more soluble iron originated from goethite which could enhance the degradation. It was also found that goethite itself was able to remove 50% of dinoseb in the presence of hydrogen peroxide in 30 minutes in an acidic environment.

BIOGRAPHICAL SKETCH

Peng Ye was born in a small mountainous village with an identical twin brother in Shanxi Province, China in 1979. After having a wonderful childhood on the mountain, in 1986, right before the age required to go to school, his whole family moved to a village located in nearby Henan Province, China, where there are better education resources and fewer mountains.

He completed his elementary and middle school in nearby village schools. In 1994, he went to the county's best high school, First High School of Linzhou, where he met a lot good teachers and friends. After spending three years in this wonderful school, in 1997, he got an admission from one of China's best university, Beijing University. During the undergraduate study, majored in Applied Chemistry, he was very interested in environmental sciences. As a result, after completing his undergraduate, he entered into a graduate program of environmental sciences, working on several projects concerning on eliminating the usage of persistent organic pesticides in China.

In the spring of 2004, with a master degree in Environmental Sciences, he received an exciting offer letter from Prof. Lemley at Cornell University. Without any hesitate, he joined the Lemley lab. This has been proved to be the best decision he had ever made by far. At Cornell, he received systematic education in Environmental Toxicology, which is a new and multi-disciplinary program. He worked on the degradation of widely used agrochemicals by anodic Fenton treatment in soil slurry systems. He very much enjoyed the working atmosphere here: nicest advisors, friendly co-workers, and best educational and experimental resources.

In the fall of 2008, after completing his PhD degree, he accepted a chemist position in a pharmaceutical company in Norwich NY, where he will deliver his expertise and knowledge in the pharmaceutical industry.

To my beloved parents, Zenglin Ye and Meihua Liu, my wife, Jun and my son, Ryan

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LIST OF ABBREVIATIONS

2,4-D:	2,4-Dichlorophenoxyacetic acid
AFT:	Anodic Fenton treatment
AOPs:	Advanced oxidation processes
CFT:	Classic Fenton treatment
DDT:	Dichloro-Diphenyl-Trichloroethane
DNOC:	4,6-o-dinitrocresol
FTIR:	Fourier Transform Infrared Spectroscopy
GC:	Gas chromatography
HA:	Humic acid
HPLC:	High performance liquid chromatography
LC-MS:	Liquid chromatography-mass spectrometry
NACs:	Nitroaromatic compounds
PNP:	p-nitrophenol
SOM:	Soil organic matter
TCE:	Trichloroethylene
TNT:	Trinitrotoluene
XRD:	x-ray diffraction

Chapter 1

Introduction

During World War II, two synthetic organic chemicals, the herbicide 2,4-D and the insecticide DDT, were introduced as defoliant and pest control reagents, respectively. Since then, more and more biologically active synthetic organic chlorine compounds, characterized by high persistence and a broad spectrum of activity, have been produced and introduced for agricultural use. However, the widespread and intensive use of these organic chlorine pesticides in the first twenty years after their introduction caused several ecological problems, including the development of resistance in pests, the elimination of natural pest controls, and the spread of persistent residues throughout different compartments of the environment and their accumulation in living systems (*1*). These problems led to the banning of DDT and other organic chlorine compounds in the 1970s in the US. A world-wide action phasing out or limiting the use of persistent organic pollutants, such as DDT, lindane and chlordane etc., was implemented as an enforcement of the Stockholm Convention in 2004.

At the same time, with the awareness of these ecological problems, more and more new, non-persistent or much less persistent chemicals effective only against the target organism were successfully developed. Organic pesticides have greatly improved the quantity and quality of food as well as the control of disease vectors and pests adversely affecting the health and welfare of human beings. However, the concerns about using more and more organic chemicals in agriculture did not diminish or go away; instead, they are still growing. The main concerns include the hazard of soil pollution by pesticides, their impact on soil fertility (*1*), their residues in food (*2*), and their potential risk of polluting surface or ground waters (*3, 4*).

1.1 Fate, transport and transformation of organic agrochemicals in soils

Each year, millions of pounds of pesticides are applied in agriculture, forestry or industry in the US (5) and have the potential to pollute various environmental media such as surface water, groundwater, and soil. Pesticide sources of soil contamination include application events, atmospheric wet or dry deposition, foliar washoff, or accidental spills onto the soil surface or into the soil profile. Environmental sinks for pesticides include chemical, photochemical and biological transformation, volatilization losses, erosion and runoff, leaching, and harvest removal and storage (6).

Overall, there are several factors that can affect the half-life and final concentration of an organic agrochemical in soil, including: retention or sorption, leaching, volatilization, biological and chemical transformation, and photochemical degradation.

Retention of organic agrochemicals in soil

As one of the key processes strongly affecting the fate and transport of organic chemicals in the soil- water environment, retention refers to the ability of the soil to retain an organic molecule and to prevent the molecule from moving either within or outside of the soil matrix (7). Retention is often referred to the adsorption process. Adsorption is a process defined as the accumulation of a gas or liquid solute on the surface of a solid, such as soil, or a liquid, and desorption is the reverse process of adsorption. There are two important factors affecting the retention of an organic chemical in a soil matrix, the nature of the soil matrix and the nature of the organic chemical.

Based on the US Soil Conservation Service (8), “soil is the collection of natural bodies of the earth’s surface, in places modified or even made by man or earthy materials, containing living matter and supporting or capable of supporting plants out

of doors. Its upper limit is air or shallow water and its lower limit is the depth to which soil weathering has been effective.” Thus, based on the components of the soil, it can be defined as a mixture of minerals, organic matter, water and air. The solid phase, including minerals and organic matter, has primary sites for chemical accumulation and transformations. The liquid phase (water) and gas phase (air) are mainly modes of transport for soluble and volatile chemicals.

Adsorption of organic chemicals on the surface of soil particles is dependent on the number and type of functional groups at accessible soil inorganic and organic surfaces. Soil inorganic components are composed of crystalline and noncrystalline, amorphous minerals, including primary and secondary minerals. On soil inorganic surfaces the main functional groups contributing to adsorption include siloxane ditrigonal cavities in phyllosilicate clays, such as montmorillonite clay, and inorganic hydroxyl groups generally associated with metal oxides, such as goethite (9). Soil organic components include polymeric organic solids, decomposing plant and animal residues, and soil organisms. However, the most studied soil organic matters are humic substances (mainly humic and fulvic acids), which have many organic functional groups, such as carboxyl, carbonyl, phenylhydroxyl, amino, imidazole, sulfhydroxyl, and sulfonic groups. When an organic molecule reacts with the surface functional groups, either an inner- or outer- sphere surface complex is formed (7). An inner-sphere complex is formed directly by the organic molecule and the surface functional groups, while, an outer-sphere complex has at least one solvent molecule, such as water, between the surface functional group and the organic molecule bound to it.

In addition to soil minerals and organic matter, soil water also plays an important role in the retention of pesticides by soil in that it is both a solvent for the pesticide and a solute that can compete for adsorption sites. Moreover, as mentioned above, soil

water is also directly involved in many adsorption mechanisms such as water bridging and ligand exchange. Soil water also carries other solutes such as Fe and Al that may be involved in cation bridging adsorption mechanisms.

The other important factor affecting the retention of an organic chemical in a soil matrix is the nature of the organic chemical. The physical and chemical properties are largely responsible for an organic chemical's behavior in soil. These properties include water solubility, pKa, pKw, polarity and functional groups, etc. For example, researchers (10) reported a significant relationship between solubilities or solvent-water partition coefficients of nonionic organic compounds and soil-water distribution coefficients. By using phenols as probe chemicals, researchers found that the type, placement and number of the functional groups determine the strength of bonding as well as the availability for bonding (11, 12). The functional groups, such as methyl or nitro groups, not only affect the pKa of the chemicals, but also affect the water solubility or solvent-water coefficient.

Adsorption-desorption is a dynamic process in which molecules are continually transferred between the bulk liquid and the solid surface. There are different adsorption mechanisms for different organic compounds. Generally speaking, organic compounds can be sorbed by physical/chemical bonding such as van der Waals forces (2-4 kJ/mol), hydrogen bonding (2-60 kJ/mol), dipole-dipole interactions, ion exchange, covalent bonding, protonation, ligand exchange, cation bridging and water bridging with varying strengths of interactions (7).

Transformations of pesticides in soil

Microbial metabolism is the primary force in pesticide transformation or degradation. Microorganisms are key agents in the degradation of various pesticide

molecules in terrestrial or aquatic systems through such processes as aerobic, anaerobic, chemolithotrophic metabolism, fermentation, and metabolism via extracellular enzymes. Microbial transformation of organic pesticides has been widely studied. Generally speaking, there are five processes involved in the microbial transformation of pesticides, including biodegradation, cometabolism, polymerization or conjugation, accumulation and secondary effects of microbial activity (13). In the biodegradation process, organic pesticides serve as substrates and the energy source for microbial growth; in the cometabolism process, the organic molecule is transformed by metabolic reactions but does not serve as an energy source for the microorganism; in polymerization or the conjugation process, organic molecules are linked together with other human synthesized or naturally occurring organic compounds; in the accumulation process, organic molecules are incorporated into the microorganism. The secondary effects of microbial activity include changes of pH, redox conditions, reactive products, etc. brought about by microorganisms in terrestrial or aquatic environments, leading to the transformation of organic agrochemicals.

Many types of reactions are involved in microbial transformation, for example, oxidative reactions, hydroxylation, N-dealkylation, decarboxylation, epoxidation and aromatic ring cleavage, etc. Usually, the microbial transformation of a pesticide involves more than one type of mechanism, and various products can be derived from the same parent compound depending on different environmental conditions.

Though microbial transformation is believed to be the main organic pollutant's transformation mechanism in soils, abiotic transformation has attracted more and more attention recently. Abiotic transformations occur in both homogeneous phases, such as the liquid phase, and in the solid-liquid interface (14). The most common reaction

organic pesticides undergo in soil solution is hydrolysis. For example, hydrolysis of esters, such as carbamates, is one of the most important hydrolysis reactions of pesticides. The soil solution contains numerous species that can produce free radicals through chemical or photochemical processes (15). Non-biological oxidation by free radicals, such as the hydroxyl radical, is another important reaction pathway for a pesticide's disappearance in soils (16). Other than hydrolysis and redox, many other transformation reactions can occur in soil solution. For example, glyphosate undergoes nitrosation to form N-nitrosoglyphosate in the presence of nitrite (17), and chlorotriazine herbicides undergo a displacement of the chlorine atom by various nucleophiles, such as OH, which is both acid and base catalyzed (18). Besides the transformation in the liquid phase, heterogeneous catalysis at the solid-solution interface, for example at the negatively charged clay surface, also plays an important role in the transformation of some pesticides in soil, such as trifluralin, parathion and others (19-21).

An increasing number of cases of pollution resulting from the leakage of toxic organic substances, including pesticides, are being detected (14). The high concentration of toxicants in these wastes often inhibits microbial degradation. Physicochemical processes such as abiotic transformations may then be responsible for the disappearance of the toxic organic substances that could endanger groundwater or surface water.

1.2 Soil remediation by chemical oxidation

Due to the leaching or runoff of pesticides from fields, pesticide-contaminated soils pose potentially serious threats to surface and ground water quality, especially when contaminant concentrations are high due to accidental spills, discharges, or leaking from storage tanks. This can be a problem at formulating and retail facilities, some of

which may qualify as superfund sites (22-24). Contaminated soils at these facilities often contain multiple pesticide active ingredients and fertilizer components. It is necessary to find effective ways to treat and remediate pesticide-contaminated soils in order to reduce or eliminate their potential threats to surface water or groundwater and to recover the soil functions. Based on EPA reports (25), there are generally four types of soil remediation methods: biological, physical/chemical, thermal, and off-gas treatment.

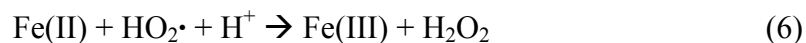
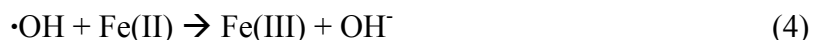
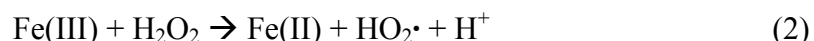
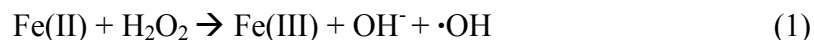
For small-scale pesticide-contaminated soils with a high concentration of organic pollutants (for example, at a pesticide accidental spill or leaking site or a pesticide formulating and retail facility), chemical oxidation is often used as a quick and effective treatment method. It can also be used as a pretreatment method followed by biological remediation. *In situ* chemical oxidation is one of several innovative technologies that shows promise in destroying or degrading an extensive variety of hazardous wastes in ground water, sediments, and soil. The oxidants used are readily available, and the treatment time is usually much shorter than that of biological methods, making the process economically feasible (26). *In situ* chemical oxidation is based on the delivery of chemical oxidants to the contaminated media in order to destroy the contaminants by converting them into innocuous compounds commonly found in nature. The oxidants applied in this process are typically hydrogen peroxide, potassium permanganate, ozone, or, to a lesser extent, dissolved oxygen.

Chemical oxidation-Fenton reaction

By far, the most common field applications of the chemical oxidation method have been based on the Fenton reagent whereby hydrogen peroxide is applied with an iron catalyst, creating a hydroxyl free radical ($\text{Fe}^{2+} + \text{H}_2\text{O}_2 \rightarrow \text{Fe}^{3+} + \text{OH}^- + \text{OH}\cdot$). Henry J. Fenton first reported this reaction in 1894, hence the name Fenton reaction. Since

then, Fenton and related reactions have become of great interest for their relevance to the chemistry of natural waters, the treatment of hazardous wastes, synthesis, and biological chemistry. A search of the topic ‘Fenton reaction’ in SciFinder yielded nearly 3000 scientific articles since 1930. Moreover, the number of articles increased quickly in the past decade from 118 articles/year in 1997 to 313 articles/year in 2007.

In 1934, Haber and Weiss (27) first proposed that the active oxidant generated by the Fenton reaction is the hydroxyl radical, one of the most powerful known oxidants. Less than two decades later, in the 1950s, Barb et al. (28-30) proposed the now-called classical or free radical mechanism for decomposition in acidic solution in the dark. The proposed mechanism consists of the sequence of following reactions:



In 1975, more than another two decades later, Walling (31) revisited and renewed the interest in Fenton chemistry among researchers in multiple fields of chemistry, such as biochemistry.

Hydroxyl radicals are nonspecific oxidants and are capable of oxidizing complex organic compounds ($\text{R-H} + \text{HO}\cdot \rightarrow \text{R}\cdot + \text{H}_2\text{O}$) at rates close to their theoretical limit, which is controlled by the rate of diffusion in water [$\sim 10^{10} \text{ l}/(\text{M} \cdot \text{s})$]. The reactions of

HO· with organic compounds lead to the formation of carbon-centered radicals. The hydroxyl radical—always present in vanishingly small concentration—reacts in well-known ways with organic compounds, principally by abstracting H from C-H, N-H, or O-H bonds, adding to C=C bonds, or adding to aromatic rings (32, 33).

The Fenton and related reactions are viewed as potentially convenient and economical ways to generate oxidizing species for treating chemical wastes. Iron is comparatively inexpensive, safe, and environmentally friendly. Hydrogen peroxide is also relatively inexpensive, safe, and easy to handle, and poses no lasting environmental threat since it readily decomposes to water and oxygen (26). This process has a history of application in waste treatment fields and is widely used in wastewater treatment (34-36). Watts and colleagues first used Fenton reagents and Fenton-like processes in degrading organic pollutants, such as pentachlorophenol, trifluralin, hexadecane, dieldrin and TCE etc., in contaminated soils (37-41). They found that Fenton or Fenton-like processes could successfully decompose those organic pollutants in surface soils. For example, they successfully decomposed high concentrations of pentachlorophenol in soil by using 7% H₂O₂ and 8 mM iron (II) at pH 3. They also found that the sorption process between organic pollutants and the soil particles played an important role in the oxidation process, and that the oxidation process and dynamics were greatly affected by the sorption and desorption processes. It was also believed that heterogeneous oxidation reactions might have occurred at the soil particle surface.

There are many kinetic models developed to describe the degradation of organic pollutants in the aqueous phase by the Fenton or Photo-Fenton process (42, 43). However, there is still no kinetic model describing the degradation process in soil by the Fenton process, likely due to the complexity of the soil media, in which soil

components and soil characteristics such as the soil organic matter, soil minerals, and soil pH may affect both the Fenton and the oxidation reactions.

Anodic Fenton Treatment (AFT) technology

In order to make the Fenton treatment method more practical and manageable, several researchers developed an innovative Fenton treatment method, called membrane Anodic Fenton Treatment technology (44, 45). The basic idea of this technology is to deliver the Fenton reagents, i.e., ferrous ion and hydrogen peroxide, continuously. Specifically, ferrous ion is delivered by electrochemical reaction through an iron electrode, and hydrogen peroxide is delivered by a peristaltic pump. This technology made a significant improvement to the classic Fenton treatment (CFT), which has two drawbacks in its application in wastewater treatment (46): one is the low pH of the effluent (the optimized pH value for CFT is about 3) that requires neutralization prior to the discharge, and the other is the handling of ferrous salts and accurately delivering the ferrous solution into the reaction system, because ferrous salt is hygroscopic and aqueous ferrous ion is readily oxidizable. Anodic Fenton treatment method has overcome these two drawbacks. The whole AFT system can be illustrated in the following scheme (**Fig 1.1**).

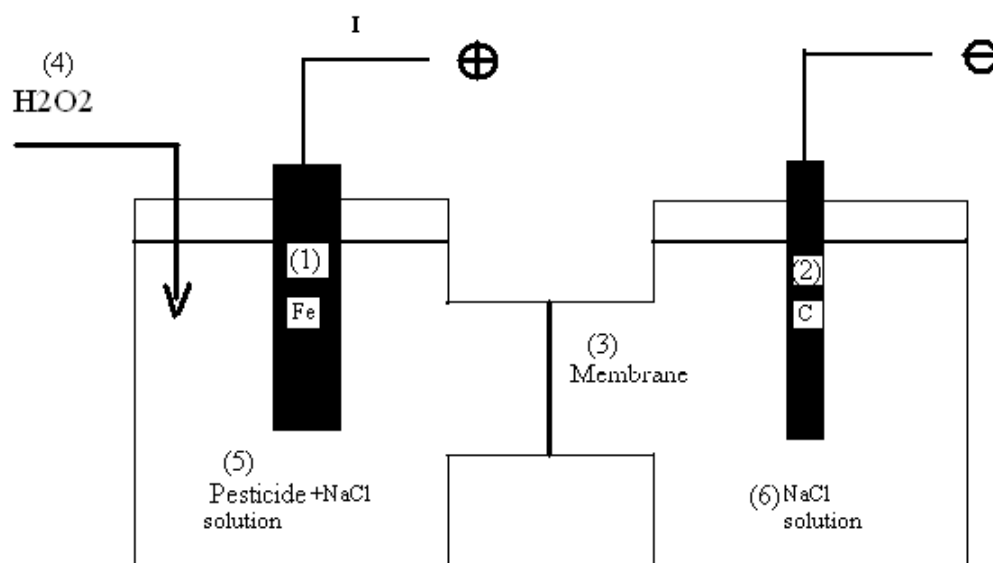
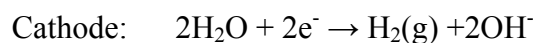
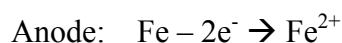


Figure 1.1 Scheme of membrane Anodic Fenton Treatment System

In the above scheme, an iron plate (1) and a graphite stick (2) are used as the anode in the anodic half-cell and the cathode in the cathodic half cell, respectively. Between the two half cells there is an anion exchange membrane (3) which only allows anion to pass through. It has been demonstrated that anion exchange membrane allows using lower electrolyte, NaCl concentration in the anodic half cells to achieve the same degradation efficiency, compared with cation exchange membrane (47). Hydrogen peroxide (4) is introduced into the anodic half cell by a peristaltic pump. Pesticide wastewater dosed with sodium chloride as the electrolyte is added to the anodic half cell (5), while sodium chloride solution (the electrolyte) is added to the cathodic half cell (6). The occurrence of pesticide degradation is restricted to the anodic half-cell. The reactions are summarized as follows:



For the above treatment method, a kinetic model (AFT model) was developed, and a

brief summary of the model is as follows (44, 45). Several assumptions were made as the basis of the model: (i) the concentration of ferrous iron in the reaction system is constant; (ii) hydrogen peroxide can be accumulated in the reaction system when the ratio of hydrogen peroxide to ferrous ion is >1 ; (iii) the Fenton reaction obeys second-order kinetics; (iv) the instantaneous concentration of hydroxyl radical is proportional to its generation rate; and (v) the kinetics of the hydroxyl radical reaction with organics are second order. The following equation was developed to describe the model:

$$\ln \frac{[C]_t}{[C]_0} = -\frac{1}{2} K \lambda \pi \omega v_0 t^2$$

In the above equation, $[C]_0$ (μM) and $[C]_t$ (μM) are the pesticide concentrations at time 0 and t min, respectively; $K=k \cdot k_I$, ($\mu\text{M}^{-2} \cdot \text{min}^{-2}$), in which k ($\mu\text{M}^{-1} \cdot \text{min}^{-1}$), and k_I ($\mu\text{M}^{-1} \cdot \text{min}^{-1}$) are the second order rate constants of the Fenton reaction and the reaction between hydroxyl radical and target compound, respectively; λ (min) and π (min) are the average lifetimes of the hydroxyl radical and ferrous ion, respectively; ω is a constant related to the delivery ratio of hydrogen peroxide to ferrous ion and to the consumption ratio of hydrogen peroxide; v_0 ($\mu\text{M} \cdot \text{min}^{-1}$) is the delivery rate of ferrous ion by electrolysis; and t (min) is time.

The AFT overcomes the two drawbacks of the classic Fenton treatment method. The Fenton reaction occurs in self-developed optimal acidic conditions (pH ~ 3) and the pH of the treatment effluent can be partially neutralized from 3 to 5 by combining the solutions from the two half-cells. Also, by using an iron plate as the ferrous ion source, the handling of large amounts of ferrous salt in practical applications is no longer needed.

Many pesticides or herbicides, such as ethylene thiourea, 2,4-D, atrazine, carbaryl and carbofuran, have been tested by this technology, and except for some pesticides with extremely low water solubility, most of them can be degraded quickly in several minutes under given experimental conditions, and the degradation processes fitted the developed AFT kinetic model quite well (44-46, 48-51).

1.3 Objectives

As discussed above, organic pollutants in soil can persist for a long time before being removed by natural biological or chemical processes. For lower levels of contamination, many organic pollutants can be cleaned by the soil ecosystem itself, posing lower potential risk for ecosystem, surface water and groundwater contamination. However, when the contamination is at a high level because of accidental spills, leakages or discharges, the contamination is obviously beyond the self-cleaning capacity of the soil system, and it is necessary to do a remediation treatment.

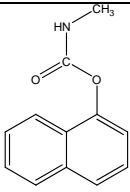
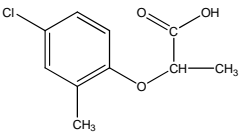
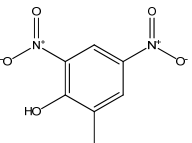
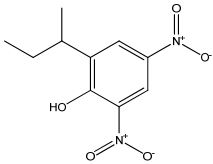
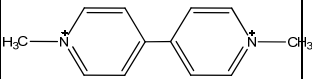
AFT is a successful lab application for degrading organic pollutants in aqueous systems. In order to further apply AFT to the treatment of contaminated soil, two preliminary studies were done on the degradation of pesticides in a slurry system. Wang and Lemley (52) showed that humic acid in a slurry that was a mimic of soil organic matter greatly affected the degradation rate and kinetics of alachlor; the authors also concluded that the shift in degradation kinetics could be attributed to the pH buffering capacity of humic acid. In another study, Kong and Lemley (53) used a real soil sample and demonstrated that 90% of 400 μM of 2,4-D was destroyed in the slurry within 20 minutes, and a two-stage degradation kinetic model was proposed. Although the effect of sorption on the degradation kinetics was discussed in both studies, this effect was not incorporated into the kinetic model, and the humic acid

used in the first study did not represent actual soil. Because of the lack of control with actual soil in the second study and the complexity of soil components, it was impossible to distinguish the effects of important individual soil properties such as soil organic matter, clays and oxides.

In this study, a synthetic soil, composed of humic acid, clay and sand, was chosen to mimic real soil, and the effect of each component was investigated. The components are all commercially available and can be easily to be controlled. The effects of each component can also be distinguished by doing control experiments.

The overall objectives of this research are: (1) to develop a kinetic model that can describe the pesticide degradation in a slurry system; (2) to identify the effects of different soil components on the AFT degradation of selected probe chemicals; and (3) to understand these effects through various mechanisms, such as adsorption or pH buffering capacity.

Table 1.1 Properties and structures of selected probe chemicals

Chemical	Water Sol. room temp., mg/L	pKa	Henry constant (p_{air}/C_{aq}), $\text{Pa m}^3\text{mol}^{-1}$	pK_w ($pK_w =$ $-\log K_w$)	Structure
Carbaryl	120	-		1.59	
Mecopro p	734	3.78	1×10^{-4}	0.1004, pH 7; 3.2 unionized	
4,6-o-dini troresol (DNOC)	6940	4.48	2.41×10^{-7}	0.08, pH 7	
Dinoseb	100	4.62			
Paraquat Cation	620,000	-	$<4 \times 10^{-9}$	-4.5	

The thesis is composed of four closely related sections, corresponding to Chapters 2 to 5. The first chapter concentrates on model development and the effect of soil organic matter on pesticide degradation, with humic acid used as a mimic of soil organic matter and carbaryl selected as a probe chemical; the second chapter focuses on the adsorption effect of 2:1 layered montmorillonite clay on the degradation of 3 selected probe chemicals, carbaryl, mecoprop and paraquat; the third chapter further investigates the adsorption effect of 2:1 layered montmorillonite clay on the

degradation of nitroaromatics, 4,6-dinitro-o-cresol and p-nitrophenol which have a special adsorption mechanism in clay in the presence of certain cations, such as K^+ or NH_4^+ ; the last chapter explores the effect of soil inorganic minerals on the AFT degradation of dinoseb, using goethite as a model mineral.

The structures and basic physical and chemical properties of selected probe chemicals are listed in the following table, **Table 1.1**.

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Chapter 2

Kinetics of Carbaryl Degradation by Anodic Fenton Treatment in a Humic Acid Amended Artificial Soil Slurry

2.1 Introduction

Each year, millions of pounds of pesticides and herbicides are used in agriculture, forestry or other industries in the US (1), leading to significant potential pollution of environmental media such as surface water, groundwater, and soil. Pesticide sources of soil contamination include application events, atmospheric wet or dry deposition, foliar washoff, or accidental spills onto the soil surface or into the soil profile (2). Due to the leaching or runoff of pesticides from fields, pesticide-contaminated soils pose potentially serious threats to surface and ground water quality, especially when contaminant concentrations are high due to accidental spills, discharges, or leakage from storage tanks. This can be a problem at formulating and retail facilities, some of which may qualify as superfund sites (3-5).

Many soil remediation methods, either physical, chemical, biological or a combination, are available for use. However, there is no perfect one, and remediation method selection should be site-, contaminant-, target- and budget-specific. Among remediation methods, advanced oxidation processes (AOPs) are often used as fast and effective treatment methods for organic chemical contaminated water or soil, due to the high efficiency and relatively low cost. One of the well documented and common field applications of AOPs is based on the Fenton reagent whereby hydrogen peroxide is applied with ferrous ion, producing hydroxyl radicals (6). Hydroxyl radicals are nonspecific oxidants and are capable of oxidizing complex organic compounds at rates

close to their theoretical limit, which is controlled by the rate of diffusion in water ($\sim 10^{10} \text{ M}^{-1} \cdot \text{s}^{-1}$) (7).

The Fenton process has a history of application in wastewater treatment (8-10). Watts and colleagues first used Fenton reagents and Fenton-like processes in degrading organic pollutants, such as pentachlorophenol, trifluralin, hexadecane, dieldrin and TCE in contaminated soils (11-16). For example, pentachlorophenol in soil was successfully degraded by using 7% H_2O_2 and 8 mM iron (II) at pH 3, and the degradation rate decreased as a function of soil organic carbon content. Degradation of various other contaminants such as TNT, heterocyclic nitramines, 2,4-D and metolachlor, and PAHs in soil has also been studied (17-22). These studies demonstrate Fenton oxidation as a promising contaminated soil remediation method.

In order to avoid highly hygroscopic and readily oxidizable ferrous salt used in classic Fenton treatment and to make the Fenton treatment method more manageable, an innovative indirect electrochemical Fenton method called anodic Fenton treatment (AFT) was developed in our laboratory (23, 24). The basic idea of this method is to generate ferrous ion electrochemically by the oxidation of an iron anode and to deliver hydrogen peroxide continuously into the anodic half cell through a pump. The AFT method has been successfully applied to degrade and detoxify many pesticides, such as ethylene thiourea, 2,4-D, carbaryl and carbofuran, etc. (23-27, 28, b, 29). Those chemicals could be removed from the aqueous system within several minutes under given conditions. A kinetic model, the AFT kinetic model was developed to describe pesticide degradation during AFT treatment in an aqueous environment (23, 24), and the model gave good fits to the degradation process.

Encouraged by the successful application of AFT in aqueous solution, two preliminary studies were done on the degradation of pesticides in a slurry system.

Wang and Lemley (30) showed that humic acid in a slurry that was a mimic of soil organic matter greatly affected the degradation rate and kinetics of alachlor, and the authors concluded that the shift in degradation kinetics could be attributed to the pH buffering capacity of humic acid. Another study, conducted by Kong and Lemley (31) and using a real soil sample, demonstrated that 90% of 400 μM of 2,4-D was destroyed in the slurry within 20 minutes, and a two-stage degradation kinetic model was proposed. Although the effect of sorption on the degradation kinetics was discussed in both studies, this effect was not incorporated into the kinetic model. Also, the humic acid used in the first study did not represent actual soil, but for the actual soil used in the second study, it is impossible to distinguish the effects of important individual soil properties such as soil organic matter and soil minerals.

Thus, an artificial soil that is a mixture of humic acid, kaolinite clay and silica sand was selected as a mimic of soil, and a widely used insecticide, carbaryl, was selected as a probe chemical in this study. Objectives of this study are: (a) to develop a kinetic model that describes carbaryl degradation in the AFT-slurry system; (b) to test the model and explain the model fitting parameters, and (c) to investigate the effects of humic acid, kaolinite clay and sand, pH, Fenton reagent delivery ratio and initial carbaryl concentration on the degradation of carbaryl during the AFT process.

2.2 Methodology

Chemicals

Carbaryl (99.5%, CAS RN 63-25-2) was purchased from ChemService, Inc (West Chester, PA). Hydrogen peroxide (30%, analytical grade), silica sand (50~70 mesh), humic acid (HA), kaolinite and catalase (EC 1.11.1.6, from Bovine liver) were from Sigma-Aldrich (St. Louis, MO). Water and acetonitrile, all HPLC grade, were from Fisher Scientific (Pittsburgh, PA), respectively. Methanol (HPLC grade), sodium

chloride and concentrated sulfuric acid (98%) were from Mallinckrodt Chemicals (Phillipsburg, NJ). Deionized water (electricity resistant, $R \geq 18.1 \text{ M}\Omega\cdot\text{cm}^{-1}$) was produced by an MP-1 Mega-PureTM system (Corning, NY)

Artificial soil and soil slurry

Silica sand, humic acid and kaolinite clay were mixed together as a model artificial soil. The weight ratio of silica sand and kaolinite clay was set as 10:9 and given amount of humic acid was added. For example, 10 g artificial soil containing 1.0% humic acid was prepared by mixing 0.1 g humic acid with 9.9 g silica sand and kaolinite clay. The artificial soil slurry was prepared by mixing given amount of artificial soil and carbaryl solution, and the ionic strength of the slurry was maintained by 0.01M CaCl_2 . Based on a preliminary adsorption kinetics study (data not shown), the adsorption equilibrium could be attained within 24 hours. The mixture was shaken for 24 hours (180 osc/min) on an Eberbach Labtools 6010 shaker (Eberbach Corporation, Ann Arbor, MI) prior to use.

Degradation of carbaryl in artificial soil slurry

All experiments were carried out in two 150-mL glass cells; a scheme of the experimental apparatus is shown in Fig. 1.1.. Typically, 100 mL of 100 μM carbaryl artificial soil slurry with 0.02M NaCl was added to the anodic half-cell, and the same volume of 0.08M NaCl solution was added to the cathodic half-cell. These two half-cells were separated by an anion exchange membrane (Electrosynthesis Company, Inc., Lancaster, NY). Each of the half-cells was well stirred by a magnetic stir bar. Ferrous ion was generated by electrolysis in the anodic half-cell from a pure iron anode (2 cm \times 10 cm \times 0.2 cm). A graphite stick (1 cm (i.d.) \times 10 cm (length)) was used as the cathode. The electrolysis current was controlled at 0.050 A by a BK Precision DC power supply 1610 (TestPath, Inc., Danvers, MA). 0.311 M hydrogen

peroxide solution was delivered to the anodic half-cell using a STEPDOS[®] Diaphragm Metering Pump (KNF NEUBERGER, Inc., Trenton, NJ) at a rate of 0.50 mL min⁻¹. When the first drop of hydrogen peroxide dropped into the anodic half-cell, the electrolysis current was turned on. Soil/solution ratio, molar ratio of H₂O₂ and Fe²⁺, initial carbaryl concentration, pH and humic acid content were kept at 1:10 (w/v), 10:1, 100 µM, pH 3 and 5.0%, respectively, unless specified, and all experiments were conducted at room temperature, 22 ± 1 °C. At given time intervals, a 0.5 mL sample was collected and added to a 1.5 mL Microfuge tube (Laboratory Products Sales, Rochester, NY) containing 0.5 mL methanol which quenched the hydroxyl radical and extracted carbaryl from the slurry in order to measure total carbaryl concentration. The sample tubes were shaken for 5 minutes on an Eberbach 6010 shaker before being centrifuged for 10 minutes at a rate of 10,000 rpm in an Eppendorf[®] MiniSpin Personal Microcentrifuge (Westbury, NY). Through preliminary experiment, by comparing the carbaryl mass before and after methanol extraction, it was found that the carbaryl extraction efficiency was >98%. The supernatant was collected for carbaryl concentration analysis. The experiments were repeated three times.

In order to measure aqueous phase concentration and total concentration over time, two anodic slurry samples, 1.0 mL and 0.5 mL, were collected simultaneously and added separately to two 1.5 mL Microfuge tubes with one containing 0.10 mL catalase solution (about 8,000 units activity) to destroy the residual hydrogen peroxide without extracting carbaryl from the solid phase and the other containing 0.5 mL methanol to quench hydroxyl radicals and extract carbaryl from the slurry. The first set of samples was centrifuged (10 minutes at 10,000 rpm) immediately after being collected, and thus reflected carbaryl concentration in the aqueous phase of the slurry; the second set reflected total carbaryl concentration in the slurry.

Carbaryl concentration measurement

The concentration of carbaryl was measured by an HP 1100 HPLC (Agilent Technologies, Inc, Santa Clara, CA) equipped with a DAD detector. The mobile phase was composed of 50% acetonitrile and 50% water (HPLC grade, pH 3, adjusted by H_3PO_4). A C_{18} 5 μm 250 mm \times 4.6 mm (i.d.) Restek reverse phase column was used. The chosen wavelength was 220 nm. Under these conditions, a clear carbaryl peak was obtained with good purity, symmetry and a retention time of 7.83 min.

Data analysis

All data analysis and model fitting work were conducted by using SigmaPlot 9.0 (Systat Software, Inc, Point Richmond, CA).

2.3 Results and Discussion

Kinetic model development.

A set of control experiments without Fenton reagents or with only ferrous ion or hydrogen peroxide and AFT batch treatment of carbaryl in the artificial soil slurry were conducted; data are shown in **Fig 2.1**. It is clear that in the absence of Fenton reagents, the carbaryl loss due to natural decomposition or adsorption on the wall of the glass reactor is negligible.

The previously developed AFT kinetic model for aqueous solution was found not to fit the experimental data, as shown in **Fig 2.1**. An empirical kinetic model was developed to simulate the pesticide degradation in the soil slurry system.

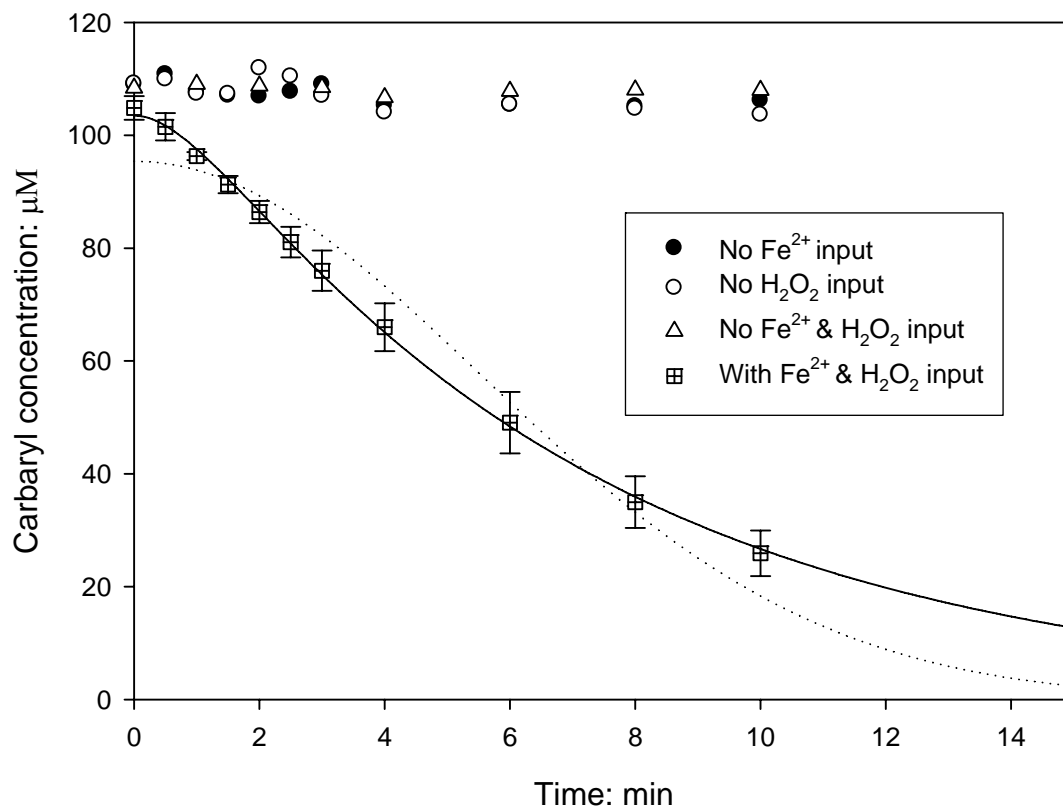


Figure 2.1 Control experiments and model fit for AFT slurry treatment data. Points are experimental data; dotted line represents model fit by AFT kinetic model for aqueous solution; solid line represents model fit by newly developed model.

In the AFT system hydroxyl radical is produced in the anodic half cell through the Fenton reaction. In the development of the AFT kinetic model for an aqueous solution system, a well justified assumption was made that, within limited treatment time, hydroxyl radical concentration is proportional to its generation rate, which is proportional to the treatment time, resulting in a linear relationship between hydroxyl

radical concentration and time (23, 24). Since the lifetime of the hydroxyl radical is extremely short and there are numerous hydroxyl radical scavengers in a soil slurry system, given enough reaction time it is reasonable to assume that the hydroxyl radical concentration will increase and approach a steady state (32) with a steady state concentration $[\cdot OH]_{ss}$ (μM). It is assumed that the hydroxyl radical concentration is increasing exponentially to a steady state, and the following mathematical equation is used to simulate this process in an AFT soil slurry system:

$$[\cdot OH] = [\cdot OH]_{ss} (1 - e^{-\lambda t}) \quad (1)$$

in which λ is a coefficient related to the production and consumption of hydroxyl radical (min^{-1}), governing the increase of hydroxyl radical concentration with time.

It is documented that the hydroxyl radical is not capable of oxidizing adsorbed organic compounds (11, 33) and the degradation reaction usually takes place in the aqueous phase, thus the degradation rate of the target compound can be written as:

$$-\frac{d[P]_{aq+L}}{dt} = k_{P,\cdot OH} [\cdot OH] [P]_{aq+L} \quad (2)$$

where $k_{P,\cdot OH}$ is the second order reaction rate constant between pesticide molecule and hydroxyl radical ($\mu M^{-1} \cdot \text{min}^{-1}$); $[P]_{aq+L}$ is the pesticide concentration in aqueous phase and labile phase (adsorbed pesticide in the labile phase can be readily desorbed from the solid phase to the aqueous phase for the degradation reaction); $[\cdot OH]$ is the concentration of the hydroxyl radical (μM). Substituting Eqn (1) into (2):

$$-\frac{d[P]_{aq+L}}{[P]_{aq+L}} = k_{P,\cdot OH} [\cdot OH]_{ss} (1 - e^{-\lambda t}) dt \quad (3)$$

In a soil slurry system, we assume that,

$$[P]_{aq+L} = [P] - \delta \quad (4)$$

where $[P]$ is the total pesticide concentration in the slurry (μM), and δ (μM) is a loosely defined constant that relates to the pesticide strongly adsorbed to the artificial soil or to pesticide in the non-labile phase; this portion of pesticide is not available for degradation within a given AFT treatment time (usually in minutes). After substituting Eqn (4) into (3) and integrating, we get the final model equation:

$$[P]_t = ([P]_0 - \delta)e^{-k_{p,OH}[\cdot OH]_{ss}[t - (1 - e^{-\lambda t})/\lambda]} + \delta \quad (5)$$

in which $[P]_0$ and $[P]_t$ are slurry pesticide concentrations at $t=0$ and t , respectively. This model equation is used to fit the experimental data and gives a very good fit as shown in **Fig. 2.1** ($R^2 > 0.99$). It should be noted that the above model is not a mechanistic model, but a loosely defined empirical model for fitting the data and measuring qualitative effects.

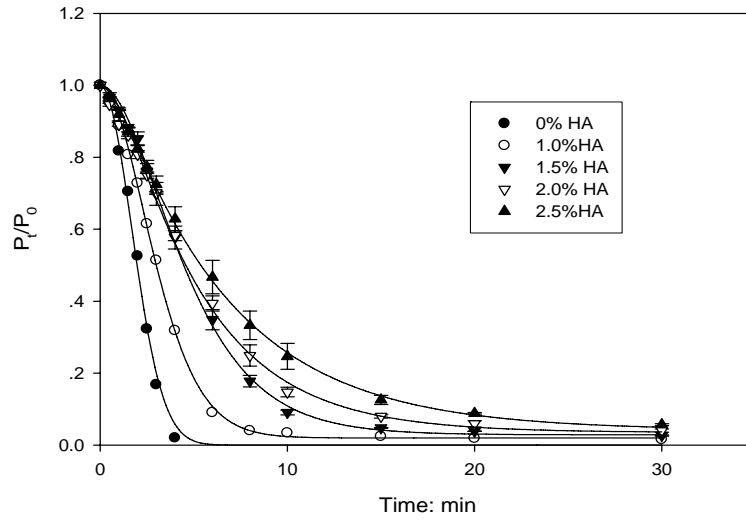
Effect of humic acid content on carbaryl degradation kinetics

Many studies have demonstrated that organic matter in wastewater or natural water bodies has an inhibitory effect on the degradation of organic pollutants (30, 34-38). Since the organic matter content in the kaolin clay and silica sand used in this experiment is undetectable, the humic acid can be considered as the only source of organic matter in the evaluated artificial soil. Initial carbaryl concentration, soil/solution ratio (w/v), and $\text{H}_2\text{O}_2/\text{Fe}^{2+}$ delivery ratio were held at 100 μM , 1:10 and 10:1, respectively. Humic acid contents (weight) of artificial soils were 0, 1.0, 1.5, 2.0 and 2.5%. The experimental results are shown in **Fig 2.2(a)**.

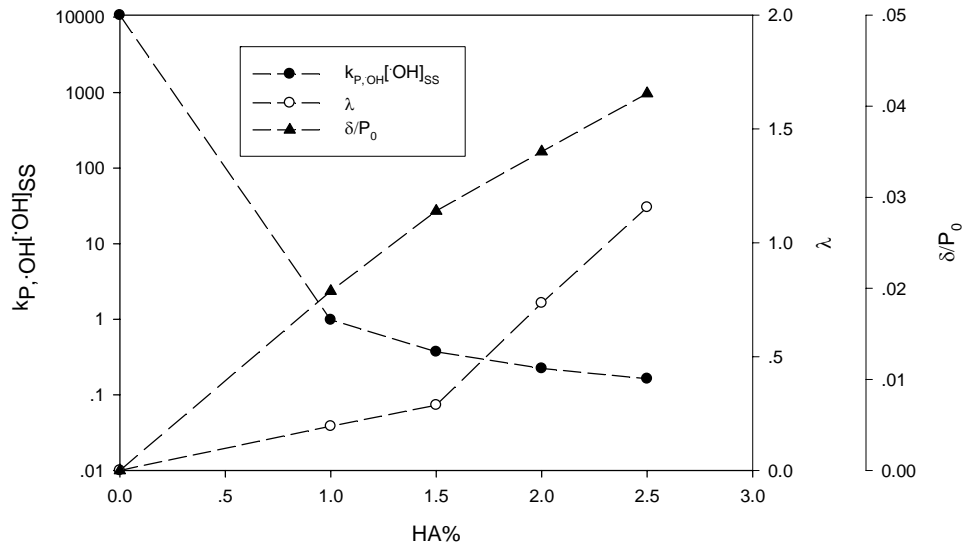
As shown in the figure, the developed kinetic model [Eqn (5)] fits the experimental data quite well ($R^2 > 0.99$). With increasing humic acid content in the artificial soil, from 0 to 2.5%, the carbaryl degradation rate slows down. In the absence of humic

acid, carbaryl concentration becomes undetectable in 5 minutes, whereas in the presence of humic acid, the carbaryl degradation is not complete (>95% removal rate) after 30 minutes of treatment. There are two possible explanations for the slowdown of the carbaryl degradation rate. One is the increased adsorption of carbaryl to the solid phase, and the other is the increased radical scavenging and chelating effect of humic acid with $\text{Fe}^{2+}/\text{Fe}^{3+}$.

In order to justify the first proposed explanation, the aqueous phase and total carbaryl concentrations in the artificial soil slurry during the AFT treatment process were compared. For the 1.0% HA slurry system, it was found that the aqueous phase carbaryl concentration became undetectable after ~6 minutes treatment, but total carbaryl concentration reached a relatively stable value as shown in **Fig 2.2(a)**. Similar results were also found for the higher HA% slurry systems, but the time to achieve the relatively stable value and the residual carbaryl concentration increased with increasing humic acid content. The results indicate that there is a certain portion of pesticide that might be strongly adsorbed to the solid phase of the soil slurry and this portion of adsorbed pesticide is not available for degradation within 30 minutes treatment time, resulting in the appearance of the relatively stable residual value. This suggests that carbaryl adsorption on the solid phase does have an inhibitory effect on total carbaryl removal in the slurry.



(a)



(b)

Figure 2.2 Effect of humic acid (HA) content on carbaryl degradation kinetics: (a) carbaryl concentration profile and kinetic model fit. Points are experimental data and lines are model fit; (b) fitting parameter analysis.

To examine if hydroxyl radical scavengers and HA's chelating effect also contribute to the decrease of carbaryl degradation rate, it is useful to note that the color of the aqueous phase of the collected samples, which reflects the color of humic acid, ferrous and ferric ions, became less intense during the treatment, from brown to nearly colorless after ~8 minutes treatment, indicating the destruction of dissolved humic acid and removal of iron species. With increasing humic acid content in the slurry, the hydroxyl radical scavenger concentration increases and iron may decrease due to the chelating effect of HA with Fe^{3+} and Fe^{2+} (39) and the blocking of Fe^{2+} regeneration from Fe^{3+} , resulting in an increased consumption rate and decreased generation rate of hydroxyl radicals. With other conditions the same, the hydroxyl radical steady-state concentration, $[\cdot\text{OH}]_{ss}$, decreases, which can explain the slowdown of the degradation. However, in order to confirm this explanation, the time scale for approaching the steady-state should be considered. Valuable information can be obtained from a model fitting parameter analysis.

The changes in the three fitting parameters, $k_{P,\cdot\text{OH}}[\cdot\text{OH}]_{ss}$, λ , and δ (or δ/P_0 for the normalized model equation) with HA% are shown in **Fig 2.2(b)**. For the first fitting parameter, $k_{P,\cdot\text{OH}}$ should be the same in all experiments since it is affected only by temperature and all experiments were conducted at the same temperature. With increasing humic acid content, $k_{P,\cdot\text{OH}}[\cdot\text{OH}]_{ss}$ decreases, (i.e., $[\cdot\text{OH}]_{ss}$ decreases), and λ and δ/P_0 increase. In the absence of humic acid in the slurry, $[\cdot\text{OH}]_{ss}$ is more than 4 orders of magnitude higher than that in the presence of humic acid. The fact that $[\cdot\text{OH}]_{ss}$ decreases with increasing humic acid content is in accordance with other researchers' results (40) and confirms that the hydroxyl radical steady-state concentration decreases with additional dissolved organic matter.

However, in the AFT system it would be more meaningful for our understanding of the treatment process if we can incorporate the time scale into the $[\cdot OH]_{ss}$ discussion, i.e., how long it will take to approach the steady state. In the model, $1/\lambda$ (min) is a parameter indicating the time scale. In the absence of humic acid, λ is very small ($<10^{-4} \text{ min}^{-1}$), which means it will take a very long time ($>10^4$ minutes theoretically) for the hydroxyl radical concentration to approach the steady state and the steady state could not be approached within the treatment time (in this study, 30 minutes). Actually, in this scenario the hydroxyl radical concentration increases linearly with time within a given treatment period (30 minutes) ($[\cdot OH] = [\cdot OH]_{ss} (1 - e^{-\lambda t}) \approx [\cdot OH]_{ss} \lambda t$). However, once humic acid is added to the slurry, λ increases. For example, λ values for 1.0, 1.5, 2.0 and 2.5% HA are 0.19, 0.29, 0.74 and 1.16 min^{-1} , respectively. If 90% of $[\cdot OH]_{ss}$ is used as the steady state approximation, the time to approach this approximate steady state can be calculated by using Eqn. (1), and the times are 12.1, 7.9, 3.1, and 2.0 minutes for 1.0, 1.5, 2.0 and 2.5% HA slurry, respectively. In other words, for the AFT treatment of soil slurry, after an “initiation” stage (at this stage, the hydroxyl radical concentration is increasing and approaching the steady state concentration) the degradation kinetics becomes pseudo-first order with respect to the steady state hydroxyl radical concentration. If the organic matter content in the system is high enough, the "initiation" step will become very short, and the entire degradation kinetics can be approximated as a pseudo-first order reaction. This is consistent with results obtained by Wang and Lemley (30), that the degradation kinetics change from classic AFT to first order with a gradual increase in humic acid content in the pesticide solution. Overall, with the increase of HA content in the slurry the hydroxyl radical steady state concentration decreases, and the decrease is most likely due to the hydroxyl radical scavenging and iron chelating effects of humic acid.

The value of δ (i.e. the residual carbaryl concentration in the slurry) increases with an increase of humic acid content in the soil slurry. In the absence of humic acid, carbaryl concentration becomes undetectable after 5 minutes and δ is close to zero, which is in accordance with the fact that there is negligible carbaryl adsorption on silica sand and kaolinite clay (data not shown). The changing trend of δ is in accordance with the findings (data not shown) that carbaryl adsorption increases with an increase of humic acid content in the artificial soil.

Effect of initial pH on carbaryl degradation kinetics

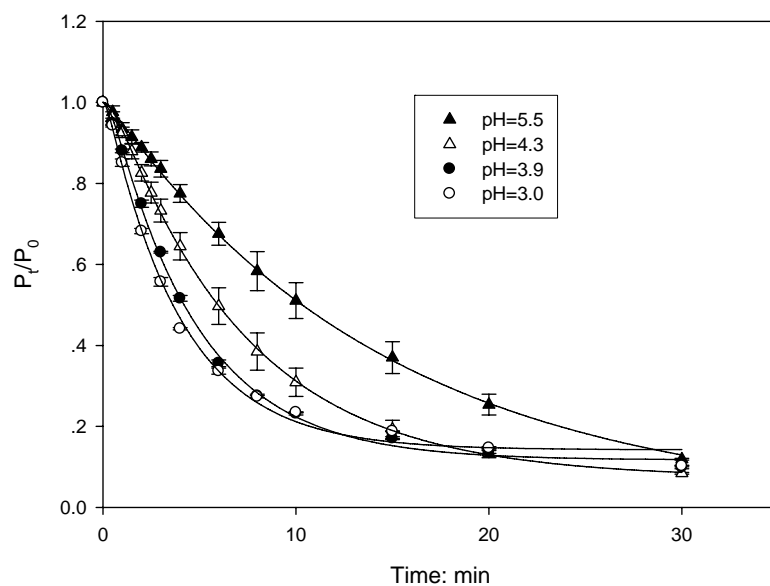
The optimum pH for the Fenton reactions is 2-3 (41, 42). In the aqueous AFT treatment this optimum pH is automatically reached after ~2 minutes treatment (24). However, a soil slurry system could be different because of the pH buffering capacity due to the protonation and deprotonation of soil minerals and organic materials (43). For example, in a soil slurry 2,4-D AFT degradation study (31), it was found that the slurry pH drops from 6.6-6.7 to ~5.6 after 2 hours of treatment, indicating a strong pH buffering capacity of the soil slurry.

The weakly carboxylic and phenolic functional groups in the soil organic matter and the hydroxy-aluminum polymers associated with the surfaces of phyllosilicates, aluminosilicates, and the edges of silicates and oxides are the main causes of the buffering. Kaolinite is a 1:1 layer clay, with very low concentrations of iron and aluminum sesquioxides and very low capacity to adsorb or provide protons, resulting in its low pH buffering capacity; thus the main pH buffering capacity of the used artificial soil in this study comes from humic acid.

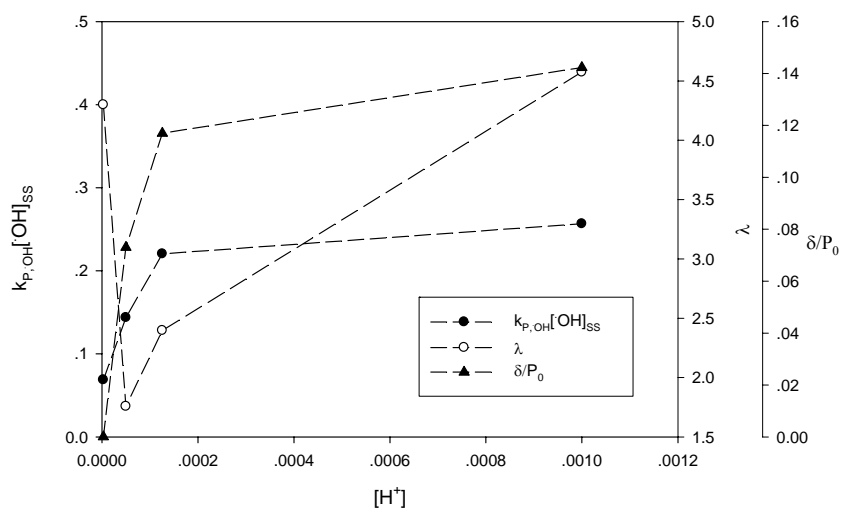
Initial carbaryl concentration, HA%, soil/solution ratio (w/v), and $\text{H}_2\text{O}_2/\text{Fe}^{2+}$ delivery ratio were held at 100 μM , 5.0%, 1:10 and 10:1, respectively. The initial pH of the slurry was adjusted to investigate its effect on the degradation of carbaryl, and

the results are shown in **Fig 2.3(a)**. The developed kinetic model fits all experimental data well. Based on the results, when the initial slurry pH was adjusted to a lower value, the carbaryl degradation rate increased compared to slurries with an unadjusted initial pH of 5.5. For example, for the unadjusted soil slurry, the initial pH was 5.5 and after 30 minutes treatment, the final pH was ~5.0, indicating the existence of the pH buffering capacity in the artificial soil and explaining why the degradation was accelerated with sulfuric acid addition.

The model fitting parameters are summarized in **Fig 2.3(b)**. It can be seen that all λ values are >1.8 , which means that the hydroxyl radical concentration can approach the steady state within 1.3 minutes after the beginning of treatment. Since the steady state can be approached quickly, the change of $[\cdot OH]_{ss}$ will greatly affect the degradation kinetics. From the figure it can be seen that $[\cdot OH]_{ss}$ increases with increasing acidity, which is in accordance with the increasing degradation rate. After the slurry pH drops below 4, $[\cdot OH]_{ss}$ does not increase much, indicating that the pH buffering capacity of the soil slurry has been overcome and that the Fenton reaction takes place in an optimum pH environment.



(a)



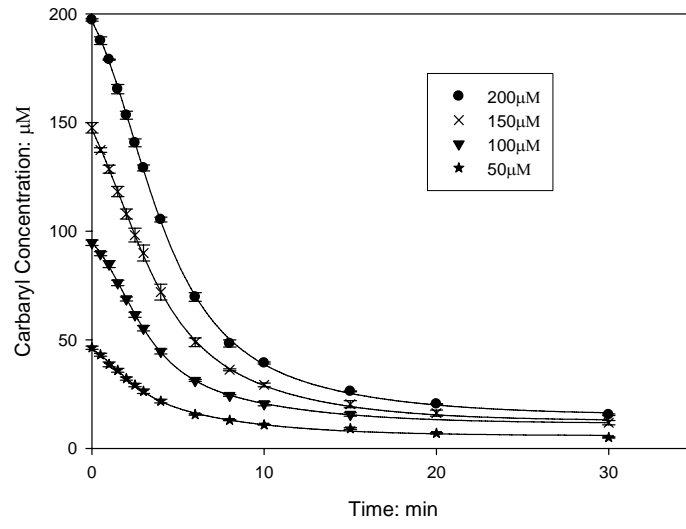
(b)

Figure 2.3 Effect of initial pH on carbaryl degradation kinetics: (a) carbaryl concentration profile and kinetic model fit. Points are experimental data and lines are model fit; (b) fitting parameter analysis.

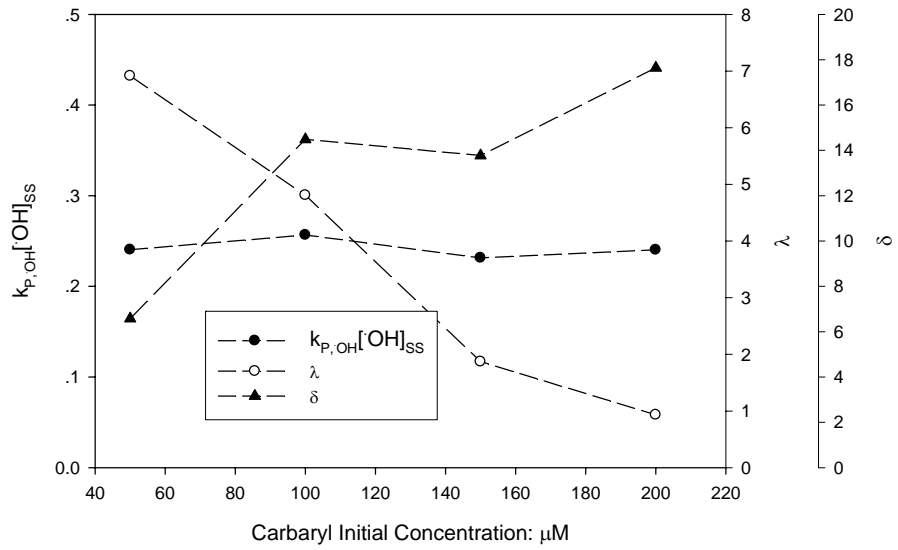
The value of δ increases with increasing initial slurry acidity (decreasing pH). Based on the adsorption experiments (data not shown), pH does not have a significant effect on the adsorption or desorption of carbaryl in a given artificial soil, indicating that the amount of carbaryl strongly adsorbed on the solid phase (not available for degradation) should be similar for slurries with the same humic acid content but different initial pH. For low initial slurry pH values, 3.0 and 3.9, the time needed to reach the relatively stable residual carbaryl concentration should be short, as is shown in the degradation curves in **Fig. 2.3(a)**, whereas, for higher pH values, 4.3 and 5.5, the time needed is greater than the treatment time, 30 minutes. Thus, the model fitting parameter, δ does not reflect the residual carbaryl concentration at the end of treatment in the case of high pH (pH>4), indicating further model optimization needed in future work.

Effect of carbaryl initial concentration on carbaryl degradation kinetics

Initial slurry pH, HA%, soil/solution ratio (w/v), and $\text{H}_2\text{O}_2/\text{Fe}^{2+}$ delivery ratio were kept at pH 3, HA 5.0%, 1:10 and 10:1, respectively, and the carbaryl initial concentration was varied to investigate its effect on degradation. The experimental results are shown in **Fig 2.4(a)**, with very good fit to the model equation. All four degradation curves reach the relatively stable value at almost the same time, around 15 minutes, with higher residual concentrations for higher initial carbaryl concentrations due to more adsorption on the solid phase. On the basis of analysis of model fitting parameters [**Fig. 2.4(b)**], all four λ values are large enough for the hydroxyl radical concentration to approach a steady state in less than 1.5 minutes, indicating a shift to first order degradation reaction shortly after the reaction begins.



(a)



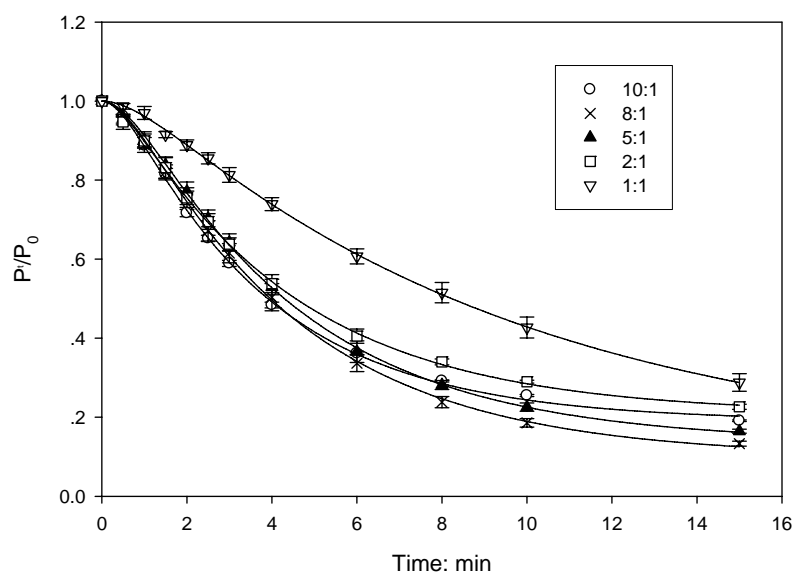
(b)

Figure 2.4 Effect on initial carbaryl concentration on its degradation: (a) carbaryl concentration profile and kinetic model fit. Points are experimental data and lines are model fit; (b) fitting parameter analysis.

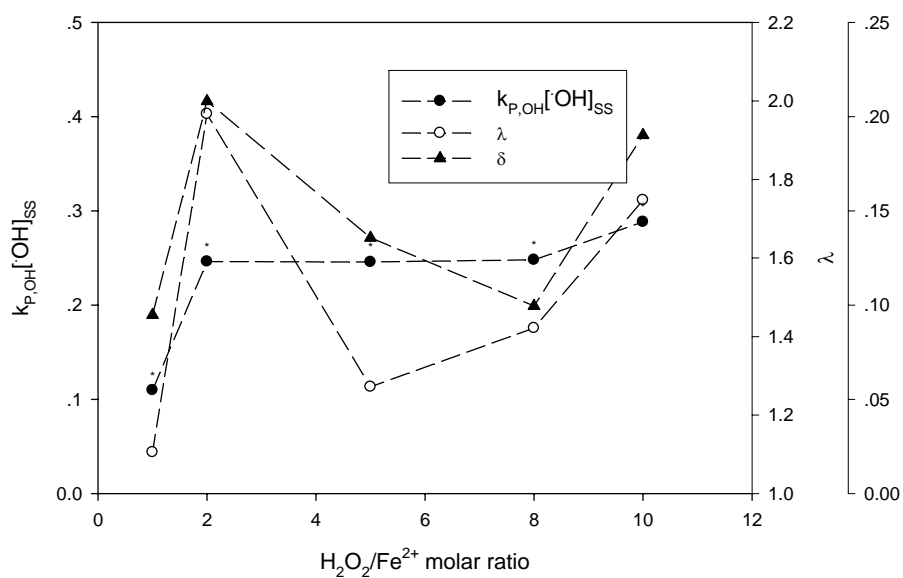
$k_{P,OH}[\cdot OH]_{ss}$ does not change with an increase of initial carbaryl concentration, indicating that $[\cdot OH]_{ss}$ is not a variable with respect to the initial pesticide concentration. Therefore, $[\cdot OH]_{ss}$ is determined by other factors such as pH, Fenton reagent delivery ratio and humic acid content. Also, since $k_{P,OH}[\cdot OH]_{ss}$ is a constant, under these conditions the AFT behaves more like a first order reaction system with a reaction rate constant $k_{P,OH}[\cdot OH]_{ss}$. Since the half life, $t_{1/2}$, of a first order reaction does not depend on the initial reactant concentration, the degradation of carbaryl in the aqueous and labile phases finished at almost the same time. δ increases with the increase of initial concentration, which is in accordance with the fact that there is more carbaryl adsorption with higher initial concentration.

Effect of $H_2O_2:Fe^{2+}$ delivery ratio on carbaryl degradation rate

The stoichiometric ratio for the Fenton reaction is $H_2O_2:Fe^{2+}=1:1$. The $H_2O_2:Fe^{2+}$ delivery ratio was increased from 1:1 to 10:1 to investigate its effect on the degradation, while initial slurry pH, HA%, soil/solution ratio (w/v), and initial carbaryl concentration were kept at pH 3, HA 5.0%, 1:10 and 100 μM , respectively. As shown in **Fig 2.5(a)**, once the ratio is greater than 1:1, the degradation curves almost overlap each other. This is an important finding from the perspective of cost since the 2:1 ratio is almost as efficient as the 10:1 ratio.



(a)



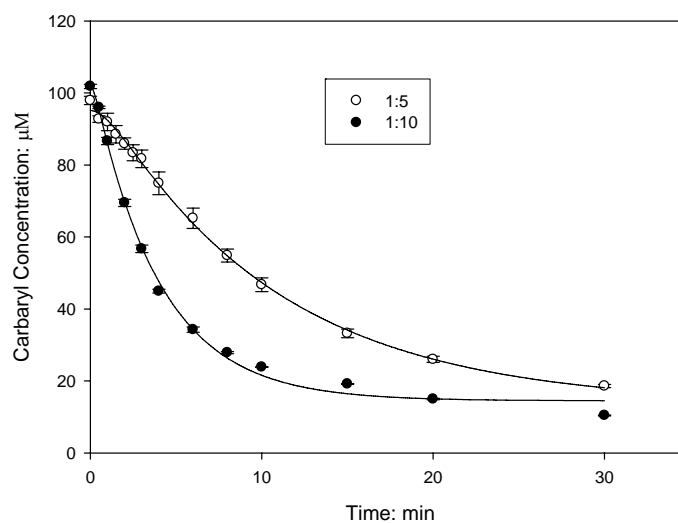
(b)

Figure 2.5 Effect of $H_2O_2:Fe^{2+}$ molar ratio on carbaryl degradation rate: (a) carbaryl concentration profile and kinetic model fit. Points are experimental data and lines are model fit; (b) fitting parameter analysis.

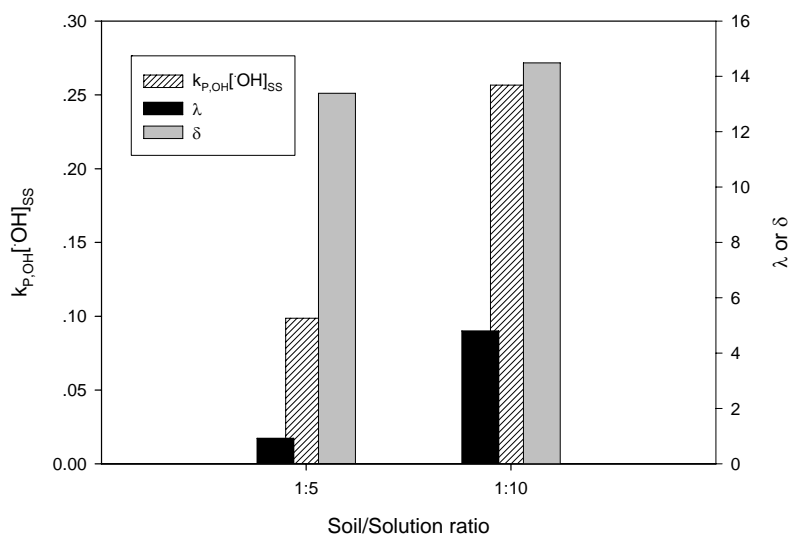
The model fitting parameter analysis [**Fig 2.5(b)**] further confirms the effectiveness of the 2:1 ratio. λ values are in the range of 1.1 to 1.9, which means that the hydroxyl radical concentration in all five reaction systems approaches a steady state within 1~2 minutes. The $k_{P, \cdot OH} [\cdot OH]_{ss}$ for the 2:1 ratio is almost double the value for 1:1, but when the ratio is increased to 3:1, 8:1, and 10:1, it does not change much, explaining the overlap of the degradation curves. Based on the above analysis, the 2:1 ratio might be most cost-effective under given experimental conditions; however, the optimum ratio may be different for different conditions, such as pH, organic matter content and clay type/content, etc., in practical application. The relationship between δ and the $H_2O_2:Fe^{2+}$ ratio is not clear.

Effect of soil/solution ratio (w/v)

The effect of soil:solution ratio on degradation was investigated. The initial slurry pH, HA%, H_2O_2/Fe^{2+} ratio, and initial carbaryl concentration were kept at pH 3, HA 5.0%, 10:1 and 100 μM , respectively. The soil:solution ratios used were 1:10 and 1:5. An attempt to use a 1:2 solution failed because sampling for pesticide analysis was not practical. The results are illustrated in **Fig. 2.6(a)**. With an increase in soil in the slurry (from ratio 1:10 to 1:5), the degradation rate decreased significantly as expected, most likely due to an increase in hydroxyl radical scavengers. The increased hydroxyl radical scavenger concentration causes the decrease in hydroxyl radical steady state concentration, which is also confirmed by the fitting parameter analysis as shown in **Fig. 2.6(b)**. Although the lower soil/solution ratio might be more efficient with respect to pesticide removal, a comprehensive cost analysis is required prior to practical application.



(a)



(b)

Figure 2.6 Effect of soil:solution ratio on carbaryl degradation rate: (a) carbaryl concentration profile and kinetic model fit. Points are experimental data and lines are model fit; (b) fitting parameter analysis.

2.4 Conclusions

An empirical kinetic model for soil slurry AFT treatment has been developed and tested through batch experiments. The model equation fits the data very well, and the analysis of the fitting parameters provides greater understanding of the pesticide degradation process in a soil slurry AFT system. Soil minerals and organic matter may affect the pesticide degradation process through their hydroxyl radical scavenging effect, iron chelating effect, pH buffering capacity and sorption capability. Generally speaking, the more soil organic matter content a soil has, the greater the inhibitory effect it will have on the degradation of pesticide in the soil slurry AFT system. Although kaolinite clay used in this study does not affect the degradation very much, with other types of clay, such as 2:1 layer clays, this might not be the case due to their high capacity to adsorb pesticide, or provide a pH buffering effect. It will be interesting and necessary to investigate the effects of different clay types or other minerals, such as oxides, on the degradation process in the future. It was also found that pesticide initial concentration did not affect the hydroxyl radical steady state concentration, with other conditions remaining the same, and from the perspective of cost-effectiveness, a 2:1 $\text{H}_2\text{O}_2/\text{Fe}^{2+}$ delivery ratio is preferred.

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Chapter 3

Adsorption Effect on the Degradation of Carbaryl, Mecoprop and Paraquat by Anodic Fenton Treatment in an Swy-2 Montmorillonite Clay Slurry

3.1 Introduction

The retention time of organic pollutants in soil varies, depending on the nature of the pollutants, the soil types and properties, and the outside environmental parameters, such as rainfall and temperature. Soil organic matter (SOM) and clay are considered two of the most important soil components affecting organic chemical movement in soil. It is well established that nonionic organic chemicals have a strong affinity to SOM (1-3), while negatively charged clays, especially 2:1 layered clays, are mainly responsible for the adsorption of cationic organic chemicals, such as paraquat and diquat, in soil through strong electrostatic attraction (4-6). Adsorption to SOM or clay particles decreases the rates of biodegradation. Studies have found that, compared to controls, biodegradation rates of quinoline (7), citrate (8), parathion (9), naphthalene (10) and benzylamine (11) were slowed down dramatically in the presence of clay minerals, either due to the clay protection of chemicals from being directly attacked by microorganisms or due to the inactivation of extracellular enzymes by clay adsorption. Due to the limited accessibility to microorganisms in soils or clay systems, organic compounds that are not strongly adsorbed by soil and should be readily biodegradable, such as fumigant ethylene dibromide (12, 13), can persist in soils for decades, even though the conditions are favorable for microbial growth and biodegradation.

Chemical oxidants are highly aggressive and small in size, making them a good option for degrading specific pollutants in heavily contaminated soils. Fenton reaction-

based chemical oxidation is one of the most studied degradation methods in waste water systems (14-17). Watts and colleagues first used Fenton reagents and Fenton-like processes in degrading organic pollutants, such as pentachlorophenol, trifluralin, hexadecane, dieldrin, and trichloroethylene in contaminated soils (18-23). Degradation of various other contaminants, such as trinitrotoluene, heterocyclic nitramines, 2,4-dichlorophenoxyacetic acid, and metolachlor, and PAHs in soil by Fenton reaction has also been studied recently (24-29). To avoid highly hygroscopic and readily oxidizable ferrous salt used in classic Fenton treatment and to make the Fenton treatment method more manageable, a more practical Fenton oxidation method, anodic Fenton treatment (AFT) was developed and tested in water systems (30-33). The AFT method has been successfully applied to degrade and detoxify many pesticides, such as ethylene thiourea, 2,4-dichlorophenoxyacetic acid, carbaryl, and carbofuran (30, 31, 33-37), in water systems.

Encouraged by the successful application of AFT in aqueous solution, two preliminary studies, were done on the degradation of pesticides in a humic acid (38) or real soil (39) slurry system. Although the effect of sorption on the degradation kinetics was discussed in both studies, this effect was not incorporated in the kinetic model. Also, it is impossible to distinguish the effects of important individual soil properties, such as soil organic matter and soil minerals, in a real soil slurry system. In order to identify the effects of soil components on the degradation of organic agrochemicals in soil slurry by AFT, a synthetic soil composed of kaolin clay, sand, and humic acid was tested in a previous study (40). It was found that kaolin clay, a 1:1 layer clay, has little effect on the degradation kinetics of carbaryl in the slurry due to its limited adsorption capacity and relatively small surface area. However, in real soils there usually is a substantial amount of 2:1 layer clay, such as smectite clays. It is important to study

degradation in slurries with this clay type that has a much higher cation exchange capacity and surface area.

In the present study Na⁺-montmorillonite source clay from the Clay Minerals Society was selected as a testing medium. Widely used agrochemicals, carbaryl, mecoprop (pKa 3.78) and paraquat, were selected as probes, representing neutral, anionic, and cationic organics, respectively. X ray diffraction (XRD) analysis was used to measure the d spacing of montmorillonite clay. The objectives of this study were: (1) to investigate the adsorption effect of layered clay on the degradation of probe chemicals in the AFT system; (2) to explain the effect through adsorption mechanisms and XRD analysis; and (3) to identify whether AFT is able to remove organic chemicals at the clay interlayer.

3.2 Materials and Experiments

Chemicals

Source clay Na⁺-montmorillonite (code: Srce_Clay_SWy-2) was obtained from the Clay Minerals Society (West Lafayette, Indiana). Carbaryl (99.5%, CAS RN 63-25-2), mecoprop (99.5%, CAS RN 7085-19-0) and paraquat CL tetrahydrate (99%, CAS RN 1910-42-5) were purchased from ChemService, Inc (West Chester, PA). Hydrogen peroxide (30%, analytical grade) is from Sigma-Aldrich (St. Louis, MO). Water and acetonitrile, both HPLC grade, were purchased from Fisher Scientific (Pittsburgh, PA). Methanol (HPLC grade), potassium chloride, sodium chloride and hydrochloric acid (37%) were purchased from Mallinckrodt Chemicals (Phillipsburg, NJ). Deionized water (electrical resistance, $R \geq 18.1 \text{ M}\Omega \cdot \text{cm}^{-1}$) was produced by an MP-1 Mega-PureTM system (Corning, NY)

Purified clay

The purification process is based on the literature (41). To obtain purified clay (<2 μm), 25 g of SWy-2 was placed in a 2 L beaker with 1.8 L of d.i. water and stirred for 8 h using a magnetic stir bar to hydrate the clay. After overnight (~18 h) settling, the supernatant suspension containing the <2 μm clay-sized particles was poured into 50 ml polyethylene centrifuge tubes and then centrifuged for 30 min at 6000 rpm. After discarding the supernatant, the purified clay sample was then quick-frozen by liquid nitrogen, freeze-dried, and stored. Cation exchange capacity of the purified clay was determined by BaCl_2 Compulsive Exchange Method (42), and the value was 78.7 meq/100g. Though there are no data available on the fraction of organic carbon on the SWy-2 clay, the organic carbon content should be minimal based on the Physical/Chemical Data for the source clay from the Clay Mineral Society.

Adsorption experiments

Adsorption batch experiments were conducted to obtain adsorption isotherms for carbaryl, mecoprop and paraquat in the clay slurry. Based on a preliminary adsorption kinetics study (data not shown), the adsorption equilibrium can be attained within 24 hours. 100.0 mg original whole clay or purified clay and 10.0 mL probe chemical solution with or without 0.02 M KCl were placed into 15 mL tubes; pH was adjusted by 0.01 M HCl if needed. After 24 h shaking, a 1.0 mL sample was placed in a 1.5 mL centrifuge vial. After 15 min-centrifuging at 10,000 rpm in an Eppendorf® MiniSpin Personal Microcentrifuge (Westbury, NY), the supernatant was collected for concentration analysis. The amount of adsorbed chemical was calculated based on the difference in aqueous concentration between the initial time and 24 h. A batch experiment for desorption of mecoprop was conducted to obtain clay samples for XRD analysis. After 24 h mixing to reach adsorption equilibrium, the clay slurry was

centrifuged, and the supernatant was decanted as much as possible. Then fresh water was added to the tube and the clay sample was remixed vigorously for the desorption experiment. An one time fresh water refill was used. 0.5 mL of sample was collected periodically for XRD analysis.

AFT batch experiments

All experiments were carried out in two 150-mL glass cells; a scheme of the experimental apparatus is shown in Fig. 1.1. Typically, 100.0 mL of probe chemical and clay slurry with 0.02M KCl was added to the anodic half-cell, and the same volume of 0.08M NaCl solution was added to the cathodic half-cell. These two half-cells were separated by an anion exchange membrane (Electrosynthesis Company, Inc., Lancaster, NY). Each of the half-cells was well stirred by a magnetic stir bar. Ferrous ion was generated by electrolysis in the anodic half-cell from a pure iron anode (0.5 cm \times 10 cm \times 0.2 cm). A graphite stick (1 cm (i.d.) \times 10 cm (length)) was used as the cathode. The electric current was controlled at 0.050 A by a BK Precision DC power supply 1610 (TestPath, Inc., Danvers, MA). Hydrogen peroxide solution (0.311 M) was delivered to the anodic half-cell using a STEPDOS[®] Diaphragm Metering Pump (KNF NEUBERGER, Inc., Trenton, NJ) at a rate of 0.50 mL min⁻¹. When the first drop of hydrogen peroxide dropped into the anodic half-cell, the electrolysis current was turned on. Clay/solution ratio, molar ratio of H₂O₂ and Fe²⁺, and pH were kept at 1:100 (w/v), 10:1, and pH 3, respectively, unless specified, and all experiments were conducted at room temperature, 22 \pm 1 °C. At given time intervals, a 0.7 mL sample was collected and added to a 1.5 mL Microfuge tube containing 0.7 mL methanol which was used to quench the hydroxyl radical and to extract probe chemicals (for carbaryl and mecoprop only) from the slurry in order to get the total concentration. The sample tubes were shaken for 15 minutes before being centrifuged for 15 minutes

at a rate of 10,000 rpm. The supernatant was collected for concentration analysis. The mass recoveries of carbaryl and mecoprop extraction were greater than 98%. For paraquat clay slurry, only the aqueous phase concentrations were measured, and a 1.0 mL sample with the addition of 0.10 mL methanol was centrifuged right after being collected. The experiments were repeated twice, unless specified.

XRD analysis

Clay thin film samples for XRD analysis were prepared by air drying several drops of clay slurry on glass slides. XRD spectra of clay films were obtained using a Scintag X-ray diffractometer equipped with Cu-K radiation. The scanning angle (2θ) ranged from 2 to 35 degrees at steps of 3 degrees per minute.

Concentration measurement

The concentrations of carbaryl, mecoprop and paraquat were measured by an Agilent 1200 HPLC equipped with a DAD detector and an Agilent 6130 Quadrupole Mass spectrometer (Agilent Technologies, Inc, Santa Clara, CA). For carbaryl and mecoprop, the mobile phase was composed of 50% acetonitrile and 50% HPLC grade water (pH 3, adjusted by H_3PO_4); for paraquat, the mobile phase was composed of 40% acetonitrile and 60% 0.14 M NaCl water (pH 3, adjusted by HCl). A C_{18} 5 μm 150 mm \times 4.6 mm (i.d.) Agilent reverse phase column was used. Flow rates were all set to 1.0 mL/min. The chosen UV wavelengths for carbaryl, mecoprop and paraquat were 220, 200 and 257 nm, respectively.

3.3 Results and Discussion

Adsorption of carbaryl, mecoprop and paraquat

Adsorption isotherms of carbaryl at pH 6.3, mecoprop at pH 7.8 and 3.0 in whole clay slurry, and mecoprop at pH 7.8 in purified clay slurry are shown in **Fig. 3.1**. All

isotherms are fitted with the Freundlich equation, $S = K_F C_e^{1/n}$ in which S (mg/g clay) is the mass of the adsorbed probe chemical per gram of clay; C_e is the equilibrium concentration of the probe chemical in aqueous solution; and K_F and $1/n$ are constants. Fitting parameters, K_F , $1/n$ and R^2 , are listed in **Table 3.1**.

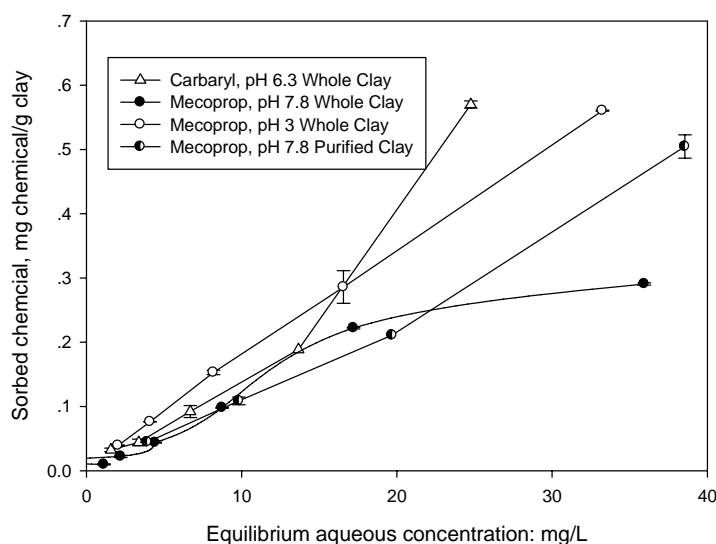


Figure 3.1 Adsorption isotherms for carbaryl (pH 6.3) and mecoprop (pH 7.8 and 3.0). Clay:solution ratio 1:100 (w/v), with 0.02 M KCl

Table 3.1 Freundlich equation fitting parameters for carbaryl and mecoprop adsorption isotherms

	K_F	$1/n$	R^2
Carbaryl, pH 6.3, Whole clay	0.00449	1.51	0.990
Mecoprop, pH 7.8, Whole clay	0.0203	0.76	0.952
Mecoprop, pH 3.0, Whole clay	0.0203	0.95	0.996
Mecoprop, pH 7.8, Purified clay	0.00734	1.157	0.994

With the same K_F (0.0203), but higher $1/n$ (0.95 vs. 0.76), the results clearly show that the neutral compound (mecoprop at pH 3.0, whole clay) has a stronger affinity to

montmorillonite clay than the anionic compound (mecoprop at pH 7.8, whole clay). Purified clay has a higher adsorption capacity than the whole clay, as indicated by its higher I/n (1.157), due to its smaller size and higher surface area.

The adsorption isotherm of paraquat with purified clay, shown in **Fig. 3.2**, appears to be a Langmuir type and thus different from the mecoprop and carbaryl isotherms, indicating different adsorption mechanisms. Strong electrostatic interaction between the cationic paraquat ions and negatively charged clay surfaces is the driving force for paraquat sorption, while for carbaryl and mecoprop other relatively weak interactions such as Van der Waals forces or hydrogen bonding are responsible for the adsorption (43). Based on the isotherm, the maximum paraquat adsorption on the purified clay is 147.5 mg/g clay, or 0.448 mmol/g clay, equivalent to 89.6 meq/100g clay, larger than the CEC of the purified clay (78.7 meq/100g) indicating that the purified clay adsorption is oversaturated.

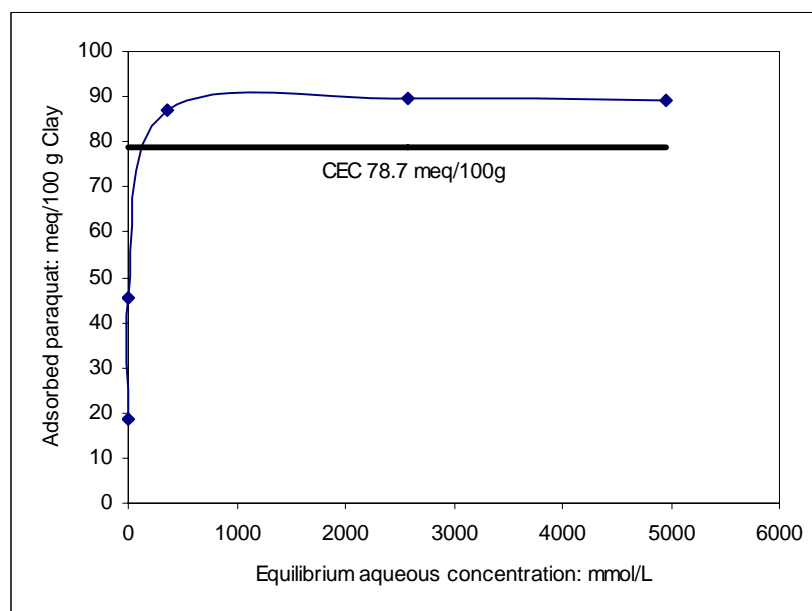


Figure 3.2 Adsorption isotherm for paraquat in purified montmorillonite clay.
Clay:solution ratio 1:100 (w/v)

To illustrate the change of clay interlayer distance caused by the adsorption of probe chemicals, the d-spacing of clay layers (d_{001}) was obtained by XRD scanning. The results are shown in **Figs.3.3 (a) and (b)** for mecoprop (0.01M KCl, pH 7.8) and paraquat (without addition of electrolyte) adsorption on purified clay, respectively.

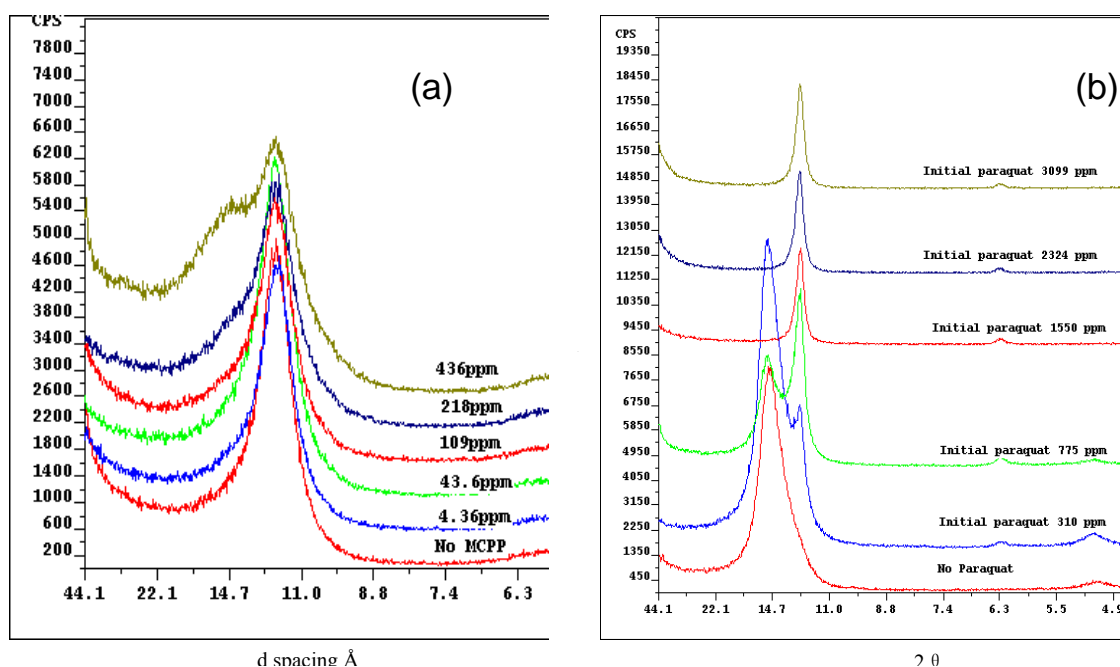


Figure 3.3 XRD of purified montmorillonite clay with different amounts of sorbed (a) mecoprop and (b) paraquat. Clay:solution ratio 1:100 (w/v), 0.02M KCl, pH 7.8; figures shown are initial probe chemical concentrations in the slurry

The initial slurry mecoprop concentrations are 0, 4.36, 43.6, 109, 218 and 436 ppm. The amounts of adsorbed mecoprop on the clay were 0, 0.04, 0.11, 0.21, 0.50, 1.19, 2.35 and 6.03 mg/g clay, respectively. For 0 to 108 ppm, there is no change in the peak or d_{001} (12.05Å). However, when the concentration reaches 218 ppm, a small shoulder peak (14.73Å) appears on the left side of the main peak, and at 436 ppm initial concentration the shoulder peak becomes clearer and stronger, indicating the inclusion of mecoprop molecules at the clay interlayer. Based on the d spacing and the

dimensions of the interlayer species, the disposition of the interlayer species can be inferred, as illustrated in **Fig. 3.4(a)** (44). For the montmorillonite clay used, the thickness of its silicate layer is about 9.6 Å (44). Without mecoprop addition, a d_{001} value of 12.05 Å is the sum of the thickness of the silicate layer and 2~3 layers of water molecules (~2.5 Å) and K^+ (the existence of a small amount of Na^+ is also possible, since the clay is not K^+ saturated). When a small amount of mecoprop is added to the clay slurry, some of the mecoprop molecules may enter the clay interlayer and be adsorbed. However, the adsorbed amount (<2 mg/g clay) is not high enough to expand the clay interlayer universally in the slurry, and the expansion is not detectable by XRD. But with an increased amount of mecoprop (>2 mg/g clay), the expanded layers become more and more universally distributed and are detected as such. The d_{001} is increased to 14.73 Å (new peak) which is about 5.1 Å greater than the silicate layer (9.6 Å); this increase is almost the same as the thickness of a mecoprop molecule, ~5 Å, as estimated by ChemBioOffice (45). This clearly indicates that a monolayer of planar mecoprop molecules (~5.1 Å) is formed at the interlayer, sitting parallel to the clay siloxane surface, which accounts for the appearance of the shoulder peak in **Fig. 3.3 (a)**.

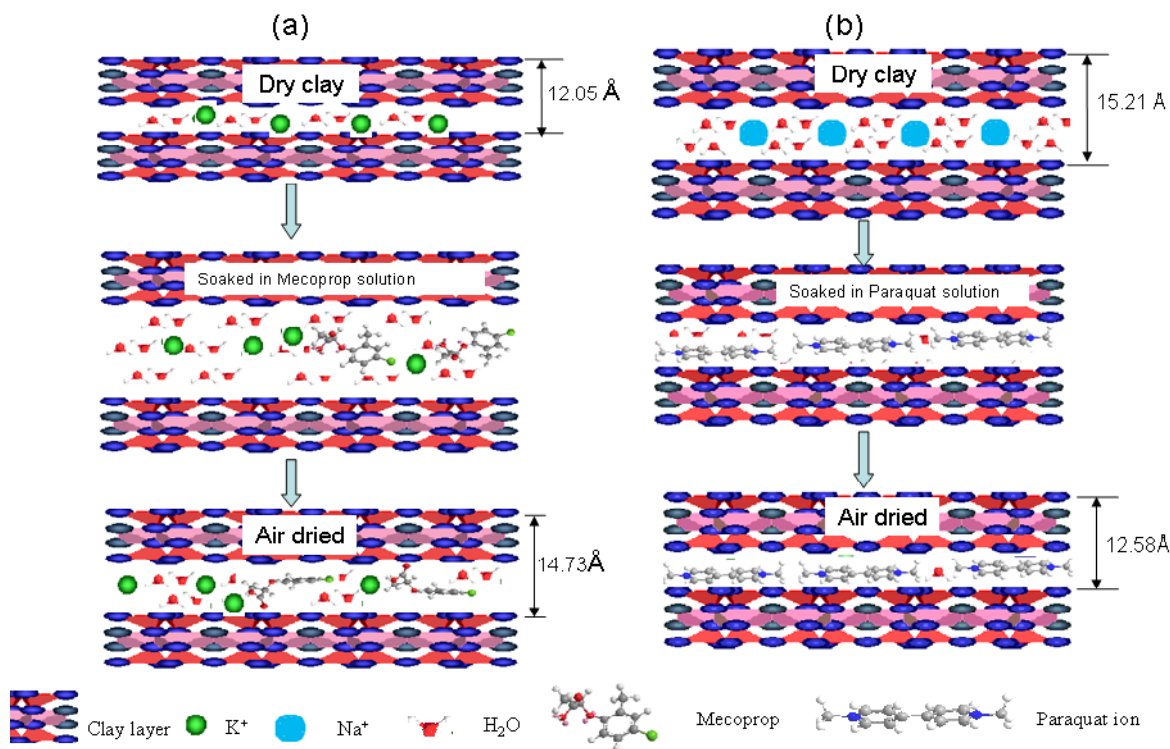


Figure 3.4 Illustration of Mecoprop (a) and Paraquat (b) adsorption on montmorillonite clay

For the paraquat case, initial concentrations are 0, 310, 775, 1550, 2324 and 3099 ppm without the addition of KCl. Based on the XRD result, without paraquat addition, the value of d_{001} is 15.21 Å. The larger d_{001} here can be compared with the d_{001} of 12.05 Å for mecoprop and is due to the larger hydration radius of Na^+ (1.85 Å) vs. K^+ (1.26 Å) (46). A shoulder peak (12.58 Å) appears on the right side of the main peak with the addition of 310 ppm paraquat. Based on the LC-MS measurement, there is no paraquat remaining in the aqueous solution, indicating complete adsorption. With the increase of initial paraquat concentration, the shoulder peak becomes stronger, while the left peak becomes weaker until it totally disappears at an initial paraquat concentration of 1550 ppm. Such a reduction in d spacing may indicate water exclusion from the clay interlayer, as reported by other researchers (47). Compared with the left peak, the width of the right peak is much smaller, indicating a very good

homogeneity of the clay sample after paraquat adsorption. The disposition of paraquat at the clay interlayer can also be inferred, as illustrated in **Fig. 3.4(b)**. After adsorption the d_{001} is decreased to 12.58\AA which is equivalent to the silicate layer plus $\sim 3\text{\AA}$, the same as the estimated thickness of a paraquat cation ($\sim 3\text{\AA}$), indicating a flat and tight disposition of planar paraquat cations at the clay interlayer. Due to the presence of paraquat and strong electrostatic forces, the clay layers come closer together, changing the clay's swelling property, as inferred by the occurrence of coagulation and flocculation of the clay particles with paraquat addition.

AFT treatment of carbaryl

Montmorillonite clay slurries with different initial carbaryl concentrations were treated by AFT, and the results are shown in **Fig. 3.5**. Carbaryl can be effectively removed from the slurry in 10 minutes at tested concentration ranges. The degradation curves were fitted with the aqueous AFT model (31) with very good correlations. This result is similar to our previous study on kaolinite clay, which found that the degradation kinetics of carbaryl in kaolinite clay slurry were not affected by the presence of the clay due to the extremely low adsorption of carbaryl.

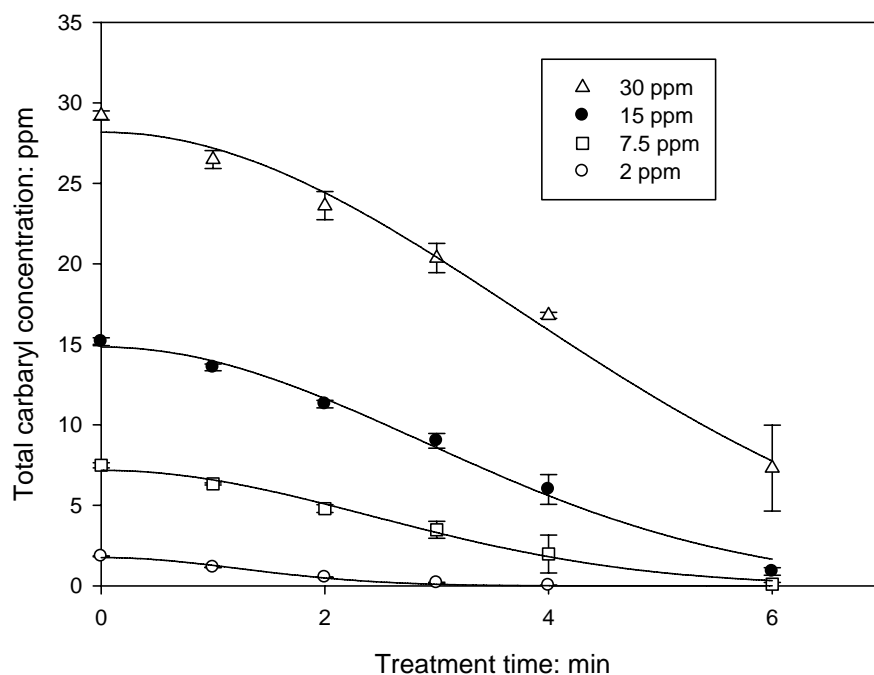


Figure 3.5 Degradation of carbaryl with different initial concentrations in montmorillonite clay slurry. Dots are experimental data and lines are fitting curves with AFT model; clay:solution ratio 1:100 (w/v), 0.02M KCl, pH 6.3

However, in both cases, the carbaryl degradation rates were lower compared with those in a pure aqueous system (data not shown), most likely due to the lower hydroxyl radical generation efficiency in the clay slurry due to the ion exchange process between clay interlayer cations and hydrogen and ferrous ions in the aqueous phase of the slurry. In typical aqueous AFT the solution pH in the anodic half cell drops quickly after treatment begins (48), a great advantage for the Fenton reaction which favors an acidic environment. However, in the presence of clay this advantage is diminished by the cation exchange process, with a resulting lower hydroxyl radical generation efficiency.

AFT treatment of mecoprop

Degradation of anionic mecoprop (pH 7.8) and neutral mecoprop (pH 3.0) in purified montmorillonite clay slurry at different initial concentrations was investigated. The results are shown in **Fig. 3.6 (a)**. Based on the figure, mecoprop can be completely degraded in the slurries at both pH 7.8 and pH 3.0 in 15 minutes at tested concentration ranges. However, at pH 3.0, the degradation rates are much faster because of the higher hydroxyl radical generation efficiency discussed in the previous section. Adsorption of mecoprop was shown to be stronger at the lower pH, but the AFT results indicate that the sorption process is not an influential factor for the degradation rates and that adsorbed mecoprop can be easily removed by AFT.

Experimental data were fitted with the slurry AFT model ($R^2 > 0.99$), and the fitting curves are shown in solid and dotted lines for pH 7.8 and 3.0, respectively. The model equation is shown below; detailed model development was documented elsewhere (40).

$$[P]_t = ([P]_0 - \delta)e^{-k_{P,OH}[\cdot OH]_{ss}[t - (1 - e^{-\lambda t})/\lambda]} + \delta \quad (1)$$

$[P]_0$ and $[P]_t$ are mecoprop concentrations (ppm or μM) at $t=0$ and t , respectively; δ is the residue mecoprop concentration (ppm or μM) that is not available for degradation at given AFT treatment time; $k_{P,OH}$ is the reaction rate constant between mecoprop and hydroxyl radical ($\text{min}/\mu\text{M}$); $[\cdot OH]_{ss}$ is the steady state hydroxyl radical concentration (μM); and λ is a coefficient related to the production and consumption of hydroxyl radical (min^{-1}).

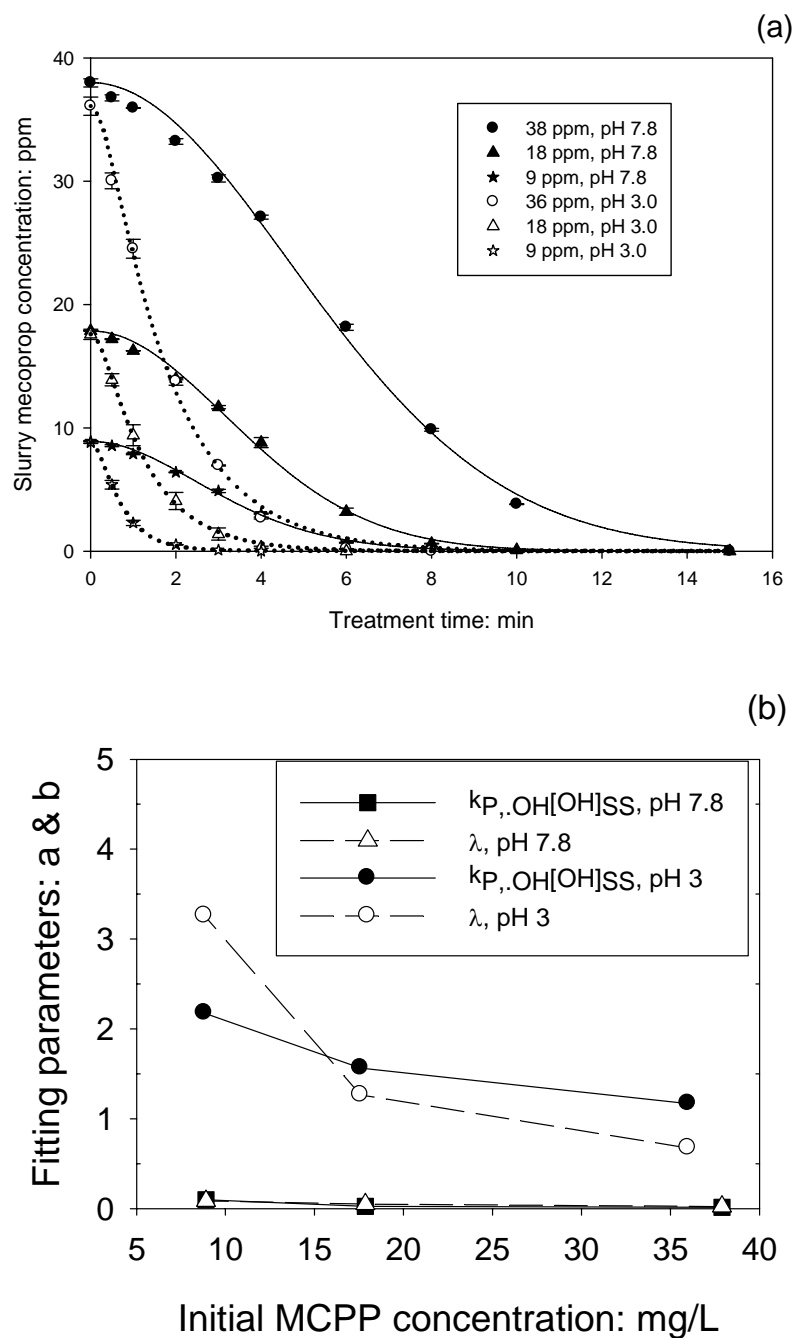


Figure 3.6 (a) Degradation of mecoprop in montmorillonite clay slurry at pH 7.8 & 3.0. Dots are experimental data and lines are fitting curves with slurry AFT model. (b) Model fitting parameters; clay:solution ratio 1:100 (w/v), 0.02M KCl

There are 3 fitting parameters for the model, $k_{P,.OH}[.OH]_{SS}$, δ and λ . Based on the fitting results, δ values are all very small ($<10^{-8}$), in accordance with complete mecoprop removal by the treatment. Values of $k_{P,.OH}[.OH]_{SS}$, and λ are plotted in **Fig. 3.6 (b)**. At lower pH, values of $k_{P,.OH}[.OH]_{SS}$, and λ are much higher, indicating higher hydroxyl radical concentration and faster approach to the steady state, resulting in faster degradation.

To further confirm that this treatment process is able to remove chemicals sitting at the clay interlayer, two clay slurry samples (clay: solution=1:100 w/v) with high mecoprop concentration (436 ppm) were prepared. The pH values of the clay slurry samples were not adjusted. The adsorbed mecoprop was about 6 mg/g clay, accounting for about 14% of total mecoprop. One clay slurry sample was treated by AFT, and samples were collected on glass slides for XRD analysis, as shown in **Fig. 3.7(a)**. Based on **Fig. 3.7(a)**, it is clear that, after the treatment begins, the left shoulder peak becomes weaker and weaker, until it totally disappears at 10 minutes; moreover, the main peak becomes sharper as treatment time increases. It should be noted that the aqueous mecoprop concentration was still high after 10 minutes AFT treatment because of its high initial concentration. This evidence clearly demonstrates that the interlayer mecoprop has been removed during the treatment process. To investigate whether the desorption process is mainly responsible for this removal or not, the other high mecoprop concentration sample underwent a desorption experiment, and samples at different desorbing time intervals were collected for XRD analysis, as shown in **Fig. 3.7(b)**. In the desorption experiment, after decanting the aqueous solution, the total mecoprop concentration in the fresh water-refilled slurry was about 60 ppm (the amount of adsorbed chemical). Based on the adsorption isotherm, at equilibrium, the majority of previously adsorbed mecoprop should return to the aqueous phase, and due to the very small amount of adsorbed mecoprop, it is not expected that the peak with a

d spacing of 14.73 Å will be detected by XRD. If the equilibrium shifts quickly, the shoulder peak with a d spacing of 14.73 Å should disappear with the shifting of equilibrium. Based on the XRD results, even after 6 h of desorption, the left shoulder peak is still strong, though it weakens with desorption time, indicating that equilibrium was not attained after 6 hours. The result suggests that the desorption rate is slower than the AFT degradation rate. This fact rules out the desorption effect as the sole removal mechanism of interlayer mecoprop. It can be reasonably inferred that interlayer mecoprop is removed by either direct attack from hydroxyl radicals or accelerated desorption in the AFT system, or by a combination of both mechanisms. Collectively, XRD results strongly confirm that AFT is capable of effectively removing interlayer mecoprop.

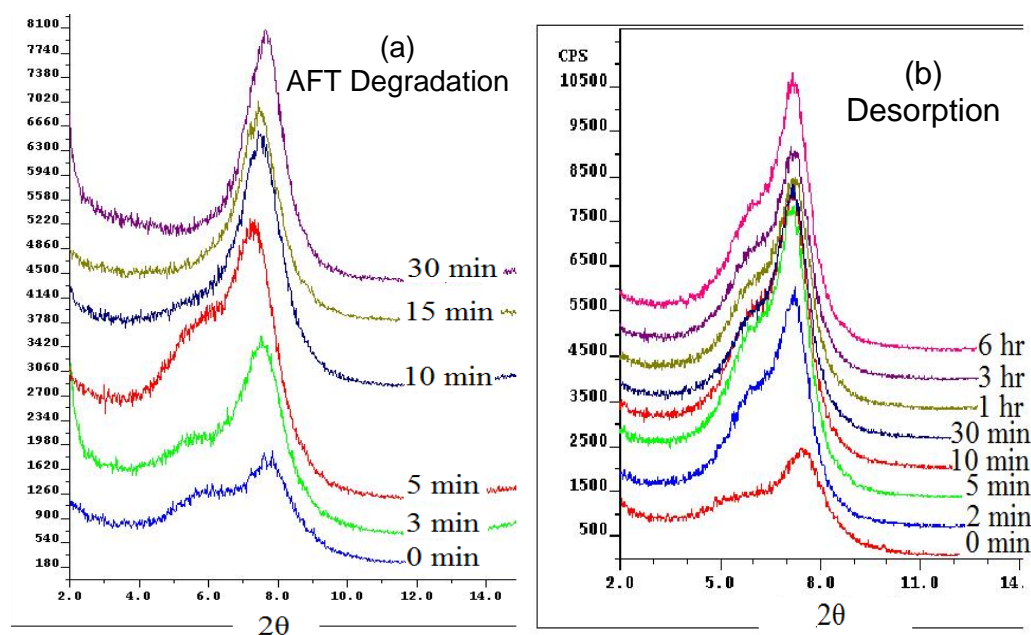


Figure 3.7 XRD analysis of montmorillonite clay during (a) AFT degradation and (b) mecoprop desorption processes; clay:solution ratio 1:100 (w/v), 0.02M KCl, pH 7.8

AFT treatment of paraquat

Due to its extremely strong adsorption, it is difficult to establish an effective method to extract paraquat from the clay slurry. In this set of AFT experiments for treatment of paraquat (initial slurry concentration: 1549.5 mg/L) and purified clay slurry (without addition of salt electrolytes), samples were collected for aqueous concentration measurement and XRD analysis, with the objective to investigate whether there is interlayer paraquat removal.

Aqueous paraquat concentration change during AFT is shown in **Fig. 3.8(a)**, and the data clearly indicate that paraquat can be effectively removed from the aqueous phase. It is interesting to note that there appears to be an increase in aqueous paraquat concentration after the treatment begins, reaching a high point at 3 minutes, before the concentration starts to decrease quickly. This anomaly in the degradation curve is believed to be due to the desorption of paraquat that is loosely adsorbed on the oversaturated clay surface as shown in the adsorption isotherm. XRD analysis of the clay is shown in **Fig. 3.8(b)**. If there were significant removal of interlayer paraquat, some of the clay layer might be re-expanded due to the removal of the strong attractive forces between paraquat and the clay layers and it should be detected by XRD. However, based on the XRD results, even after 1 h AFT treatment, the d_{001} peak remains sharp and unchanged, indicating no or very limited interlayer paraquat removal.

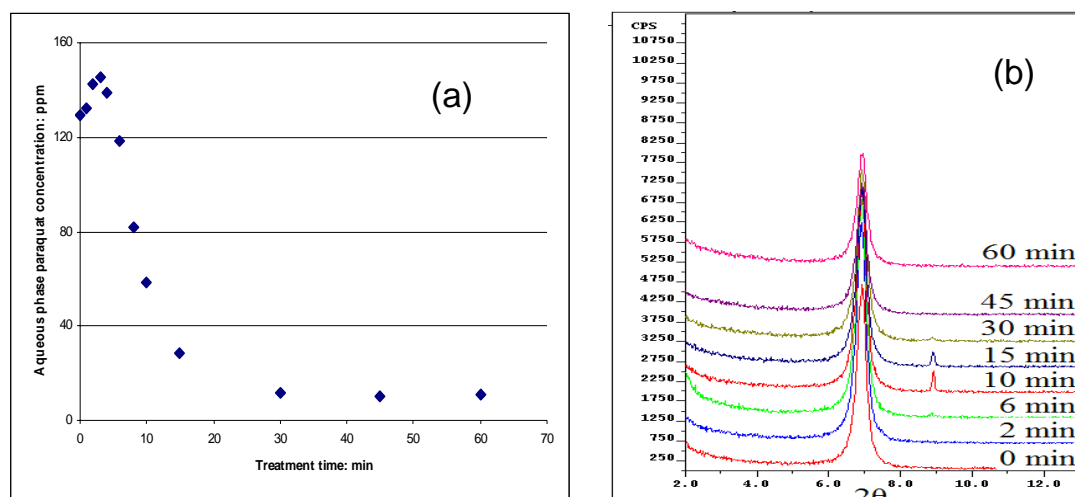


Figure 3.8 (a) Aqueous paraquat concentration, and (b) XRD analysis of montmorillonite clay, during AFT degradation process. clay:solution ratio 1:100 (w/v), no KCl addition

Based on the degradation results of these three widely used agrichemicals, we conclude that the AFT is capable of degrading carbaryl and mecoprop completely from the clay interlayer, while interlayer paraquat could not be removed by AFT. This study of the adsorption and degradation behaviors of carbaryl, mecoprop and paraquat, in a Swy-2 montmorillonite clay slurry is useful for understanding potential remediation methods. Based on their chemical properties the chemicals can be divided into two groups: neutral and anionic (carbaryl and mecoprop) and cationic (paraquat). Carbaryl and mecoprop have a weak affinity to Swy-2 clay. For the highest tested initial concentration of mecoprop in the adsorption experiments, 535.0 ppm, the amounts of sorbed mecoprop on the clay are 8.0 mg/g clay (pH 7) and 12.6 mg/g clay (pH 3.0), far less than the maximum amount of sorbed paraquat, 147.5 mg/g clay. The dipole-dipole force or hydrogen bonding is one of the most important mechanisms believed to be responsible for the adsorption of neutral carbaryl and mecoprop molecules and mecoprop anions on the montmorillonite surface. Through *ab initio*

simulation (49), researchers have found that, in the presence of water molecules and due to hydration, formation of complexes (cations as bridges connecting organics and clay surfaces) between counter ions and organic anions (2,4-D) is not preferred; however, there are three types of hydrogen bonding formed among species (water and 2,4-D anions) at montmorillonite surfaces. They are hydrogen bonds among water molecules themselves, between water molecules and the 2,4-D anions, and between water molecules and the clay basal siloxane oxygen atoms. Apparently water molecules act as a bridge between 2,4-D anions and the clay surface. Mecoprop has a structure and functional groups similar to 2,4-D, and the carbaryl molecule also has the nitrogen and oxygen atoms necessary for forming hydrogen bonds. Therefore, hydrogen bonding should be an important adsorption mechanism for these two chemicals.

Through XRD analysis, though it was found that sorbed mecoprop forms a monolayer between montmorillonite clay layers, it should be noted that the XRD sample was air-dried, which was different from the original clay slurry sample. In an air-dried sample, there are limited water molecules between clay layers, while in the slurry sample, the clay is soaked with water and the clay is swelling. Through computer simulations (50, 51) it was found that non-cationic organic molecules show a tendency to remain completely in the expanded interlayer aqueous phase, if the clay was soaked with water. In the slurry, due to the swelling of layered montmorillonite clay, Fenton reagents are able to actually enter into this interlayer aqueous phase. As a result, hydroxyl radicals can be generated locally at the clay interlayer aqueous phase, and interlayer organic molecules can be attacked by the interlayer-produced hydroxyl radicals. This is believed to be the main reason for the quick and complete removal of mecoprop from the clay interlayer, as shown in the experimental data.

Paraquat has a completely different scenario. As stated previously, with the addition of paraquat to the montmorillonite clay slurry the expanded clay began to shrink, squeezing out water molecules from the interlayer, and coagulation, flocculation and precipitation occurred. Due to the lack of enough water molecules, Fenton reagents are not able to enter into the clay interlayer and there are no interlayer-produced hydroxyl radicals. As a result, the removal of interlayer paraquat is none or quite limited, as shown by XRD analysis.

These findings may benefit our understanding of the fate, transport and transformation of organic pollutants in soil and have important implications for selecting soil remediation strategies. Except for nitroaromatic compounds, which have distinct adsorption mechanisms on smectite clay (52), for most other neutral or anionic organic pollutants, their adsorption on soil organic matter (SOM) generally outweighs their adsorption on clays, and SOM is a more important factor to study the fate and transport of organic pollutants in soil. For cationic organic chemicals, their adsorption on clay will be more important, especially in soils with a large content of layered clays with high CEC since they cannot be removed effectively by AFT at the clay interlayer. The Fenton reaction-based AFT process is capable of removing neutral or anionic organic chemicals adsorbed at the clay interlayer effectively, which is an advantage over bioremediation methods as discussed in the Introduction. The AFT method is an effective and reliable option for treatment, on a small scale, of soils that are highly contaminated by organic pollutants.

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Chapter 4

Adsorption Effect on the Degradation of 4,6-o-dinitrocresol and p-nitrophenol in a Montmorillonite Clay Slurry by AFT

4.1 Introduction

Nitroaromatic compounds (NAC) are primarily released into environmental media from anthropogenic sources. They are usually used as pesticides, explosives or azo dyes, and some are also products of the incomplete combustion of gasoline and diesel fuel (*1*). As widely used pesticides, dinitrocresol, dinoseb, parathion and methyl parathion are intentionally released into soil and water through direct application, and may also be spilled accidentally during transportation or agricultural use.

It is well established that, compared with soil clay and minerals, nonionic organic chemicals have a much stronger affinity for soil organic matter (*2-4*). However, recent studies (*5-8*) have found that negatively charged smectite clays are capable of adsorbing nitroaromatic compounds in unexpectedly large amounts. It was believed that two categories of surface sites, nonpolar and polar, are involved in NAC adsorption on clay minerals (*8*). Nonpolar sites are on the neutral siloxane surface, which are believed to be hydrophobic and important for the sorption of neutral organic compounds; polar sites originate from isomorphic substitution sites and from broken edges.

In the presence of K^+ or Cs^+ at the clay interlayer, the strong adsorption of NACs on smectites is governed by at least two important factors. One factor is the accessibility of those neutral hydrophobic sites at clay surfaces for NACs molecules. At the smectite interlayer, due to the hydration of interlayer cations, those sites are often

blocked by water molecules. For those cations with lower hydration energy and smaller hydration radius, such as K^+ and Cs^+ , it is relatively easy for organic molecules to replace interlayer molecules, accessing those hydrophobic siloxane sites. However, it is believed that there is another more important factor affecting adsorption, the interaction between cations and NACs molecules. Boyd, et al (5) and Johnston, et al (6) found that there is strong interaction between interlayer K^+ and $-NO_2$ groups on NACs, which was verified by FTIR spectra data and computational simulation. They also found that other cations, such as Na^+ , Mg^{2+} and Ca^{2+} , did not interact with $-NO_2$ groups based on the FTIR spectra data, because of the stronger hydration and larger hydration radii of these cations. They concluded that the strong adsorption of NAC on K^+ -smectite was mainly due to the formation of a complex between K^+ and NACs. These findings offer researchers a better understanding of the adsorption of NACs on layered clays and their retention in soil as well.

The strong adsorption of NACs on layered clays will greatly affect their fate and transport in soils. Based on previous studies (5-8), adsorbed NAC molecules stay firmly at the clay interlayer, which greatly decreases their bioavailability to microorganisms and increases their retention time in soils. For remediation of heavily NAC contaminated soils, the chemical oxidation method is a good option due to the high aggressiveness and small size of the chemical oxidants, e.g., hydroxyl radicals.

In a companion study (9) from our laboratory, the adsorption and degradation of carbaryl, mecoprop and paraquat in an Swy-2 montmorillonite clay slurry was investigated. Results demonstrated that anodic Fenton treatment (AFT) is a reliable method to degrade non-cationic carbaryl and mecoprop at the clay interlayer, though interlayer paraquat cations could not be removed due to their inaccessibility to Fenton reagents. Results also showed that different adsorption mechanisms affected the

degradation; specifically, the adsorption of carbaryl and mecoprop through hydrogen bonding and weak van der Waals forces has much less effect on the degradation than the adsorption of paraquat through strong electrostatic forces.

NACs have a unique adsorption mechanism on smectite clays, as mentioned above, which drives a large amount of adsorption on clay surfaces in the presence of specific cations, e.g., K^+ and Cs^+ . To the best of our knowledge, there is no research to investigate the effect of this adsorption mechanism on the degradation of NACs by chemical oxidation, which is important for selecting remediation strategies for NAC contaminated soils.

In the present study, Na^+ -montmorillonite source clay from the Clay Minerals Society was selected as a testing medium, and 4, 6-*o*-dinitrocresol (DNOC) and *p*-nitrophenol (PNP) were selected as two probes representing NACs. The objectives of this study were: (a) to investigate the adsorption effects of montmorillonite clay on the degradation of probe chemicals in the AFT system; (b) to identify DNOC degradation intermediates and illustrate DNOC degradation pathways in the AFT system, and (c) to identify whether AFT is able to remove NACs at the clay interlayer.

4.2 Materials and Experiments

Chemicals

Source clay, Na^+ -montmorillonite (code: Srce_Clay_SWy-2), was obtained from the Clay Minerals Society (West Lafayette, Indiana). 4, 6-*o*-dinitrophenol (99.5%) was purchased from ChemService, Inc (West Chester, PA). *p*-nitrophenol (99%) and hydrogen peroxide (30%, analytical grade) were purchased from Sigma-Aldrich (St. Louis, MO). Water and acetonitrile, both HPLC grade, were purchased from Fisher Scientific (Pittsburgh, PA). Deionized water (electrical resistance, $R \geq 18.1 \text{ M}\Omega \cdot \text{cm}^{-1}$) was produced by an MP-1 Mega-PureTM system (Corning, NY).

Purified clay

The purification process is based on the literature (10). To obtain purified clay (<2 μm), 25 g of SWy-2 was placed in a 2 L beaker with 1.8 L of d.i. water and stirred for 8 h using a magnetic stir bar to hydrate the clay. After overnight (~18 h) settling, the supernatant suspension containing the <2 μm clay-sized particles was poured into 50 mL polyethylene centrifuge tubes and then centrifuged for 30 min at 6000 rpm. After discarding the supernatant, the purified clay sample was then quick-frozen by liquid nitrogen, freeze-dried, and stored.

Adsorption experiments

Adsorption batch experiments were conducted to obtain adsorption isotherms for DNOC and PNP in the clay slurry. Based on a preliminary adsorption kinetics study (data not shown), the adsorption equilibrium can be attained within 24 hours. 50.0 mg purified clay and 10.0 mL probe chemical solutions with different electrolytes were placed into 15 mL tubes; pH was adjusted by 0.01 M HCl if needed. After 24 h shaking, a 1.0 mL sample was collected, and after 15 min-centrifuging at 10,000 rpm, the supernatant was collected for concentration analysis. The amount of adsorbed chemical was calculated based on the difference in aqueous concentration between the initial time and 24 h.

AFT batch experiments

All experiments were carried out in two 150-mL glass cells; a scheme of the experimental apparatus is shown in Fig. 1.1. Typically, 100.0 mL of probe chemical and clay slurry with 0.02M KCl was added to the anodic half-cell, and the same volume of 0.08M NaCl solution was added to the cathodic half-cell. These two half-cells were separated by an anion exchange membrane (Electrosynthesis Company, Inc., Lancaster, NY). Each of the half-cells was well stirred by a magnetic stir bar. Ferrous

ion was generated by electrolysis in the anodic half-cell from a pure iron anode (0.5 cm × 10 cm × 0.2 cm). A graphite stick (1 cm (i.d.) × 10 cm (length)) was used as the cathode. The electric current was controlled at 0.050 A by a BK Precision DC power supply 1610 (TestPath, Inc., Danvers, MA). Hydrogen peroxide solution (0.311 M) was delivered to the anodic half-cell using a STEPDOS[®] diaphragm metering pump (KNF Neuberger, Inc., Trenton, NJ) at a rate of 0.50 mL min⁻¹. When the first drop of hydrogen peroxide dropped into the anodic half-cell, the electrolysis current was turned on. Clay/solution ratio, molar ratio of H₂O₂ and Fe²⁺, and pH were kept at 1:100 (w/v), 10:1, and pH 3, respectively, unless specified, and all experiments were conducted at room temperature, 22 ± 1 °C. At given time intervals, a 0.7 mL sample was collected and added to a 1.5 mL tube containing 0.7 mL acetone which is used to quench the hydroxyl radical and to extract probe chemicals from the slurry in order to get the total concentration. The acetone extraction efficiency of DNOC and PNP extraction were greater than 99%. The experiments were repeated twice.

XRD analysis

Clay thin film samples for XRD analysis were prepared by air drying several drops of clay slurry on glass slides. XRD spectra of clay films were obtained using a Scintag X-ray diffractometer equipped with Cu-K radiation. The scanning angle (2θ) ranged from 2 to 35 degrees at steps of 3 degrees per minute.

Concentration measurement

The concentrations of DNOC and PNP were measured by an Agilent 1200 HPLC equipped with a diode array detector (Agilent Technologies, Inc, Santa Clara, CA). For DNOC, the mobile phase was composed of 80% acetonitrile and 20% HPLC grade water (pH 3, adjusted by phosphoric acid). For PNP, the mobile phase was composed of 50% acetonitrile and 50% HPLC grade water (pH 3, adjusted by

phosphoric acid). A carbon eighteen 5 μm 150 mm \times 4.6 mm (i.d.) Agilent reverse phase column was used. Flow rates were all set to 1.0 mL/min. The chosen UV wavelengths for DNOC and PNP were 269 and 317 nm, respectively.

Identification of DNOC degradation intermediates

In order to get a higher concentration of degradation intermediates, 100 mg/L DNOC with 0.02 M KCl solution was treated by AFT. Electric current and H_2O_2 concentration were controlled at 0.01 Amp and 0.0662 M. 1.0 ml samples were collected periodically during the treatment, and 0.1 mL methanol was added to quench hydroxyl radicals. The sample was analyzed by an Agilent 1200 HPLC with an Agilent 6130 Quadrupole Mass spectrometer. The analysis conditions are as follows: Gradient mobile phase: 0-10 min 50% H_2O (pH 3 adjusted by acetic acid), 10-15 minutes, acetonitrile increased from 50% to 100 % at a rate of 10% per minute, 50% acetonitrile, 15-26 min 100% acetonitrile; Mobile phase flow rate, 0.5 ml/min; Column: C_{18} 5 μm 150 mm \times 4.6 mm (i.d.) Agilent reverse phase; Mass spectrometer mode: ES+APCI Multi Mode; drying gas (N_2) flow rate, 12.0 L/min; nebulizer pressure, 40 psig; drying gas temperature, 350 $^\circ\text{C}$; vaporizer temperature: 250 $^\circ\text{C}$.

Nitrogen measurement

In order to check whether there were nitro groups being broken down from DNOC molecules, nitrogen concentration in the forms of $\text{NO}_3^-/\text{NO}_2^-$ and NH_4^+ were measured during the AFT treatment of DNOC solution (AFT operating conditions were the same as those described above). The analysis was conducted by a Bran+Luebbe Automated Injection Ion Analyzer (Bran + Luebbe Inc., Delavan, WI) at the Cornell Nutrient Analysis Laboratory.

4.3 Results

Effect of electrolytes on the adsorption of DNOC and PNP

Since the clay is negatively charged, the metal cations in the solution will enter the clay interlayer through the cation exchange process. DNOC adsorption isotherms in Swy-2 clay slurry (pH 3.25) with different electrolytes, 0.02 M NH_4Cl , 0.01 M CaCl_2 , 0.02 M KCl or 0.02 M NaCl , are shown in **Fig. 4.1**. It is important to note that two different scales were used for the x-axis, the top one for KCl and NH_4Cl and the bottom one for CaCl_2 and NaCl . All isotherms were fitted with the Freundlich equation, $S = K_F C_e^{1/n}$, in which S (mg/g clay) is the mass of adsorbed probe chemical per gram clay; C_e is the equilibrium concentration of the probe chemical in aqueous solution; and K_F and $1/n$ are constants. The fitted parameters, K_F , $1/n$, and R^2 , are summarized in **Table 4.1**. It can be seen that DNOC adsorption in the different

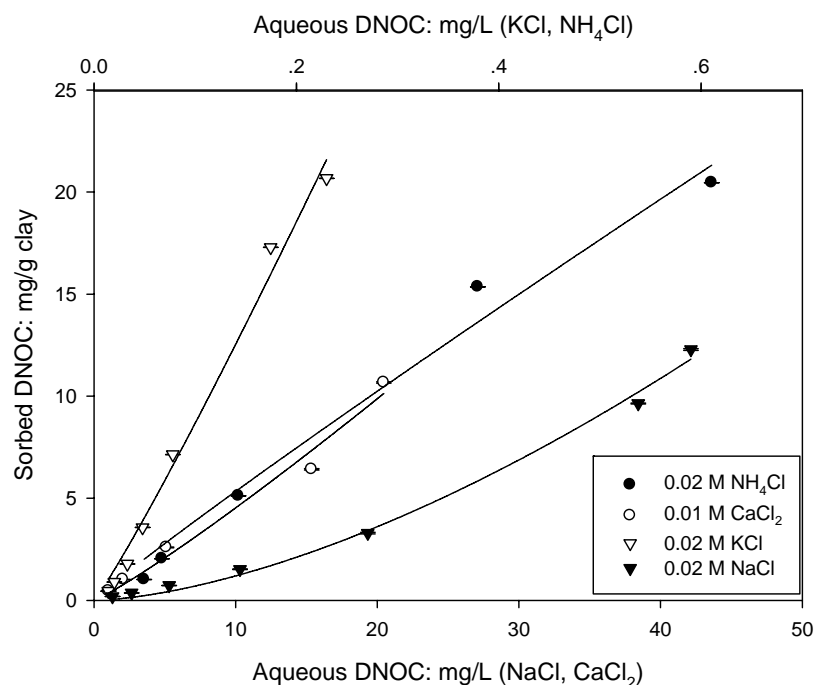


Figure 4.1 Effect of electrolytes on DNOC adsorption on Swy-2 clay

Table 4.1 Freundlich equation fitting parameters for DNOC and PNP adsorption isotherms

	K_F	$1/n$	Adjusted R^2
DNOC, 0.02 M NH_4Cl	33.9	0.94	0.98
DNOC, 0.01 M CaCl_2	0.34	1.12	0.98
DNOC, 0.02 M KCl	108.1	1.10	0.99
DNOC, 0.02 M NaCl	0.031	1.59	0.99
PNP, 0.02 M KCl	0.0143	1.19	0.97
PNP, 0.02 M NaCl	0.0005	1.55	0.98

electrolytes follows the order: $\text{KCl} > \text{NH}_4\text{Cl} > \text{CaCl}_2 > \text{NaCl}$. At pH 3.25, DNOC adsorption in KCl and NH_4Cl electrolytes is more than two orders of magnitude larger than that in CaCl_2 or NaCl. This result can be partially explained by looking at the estimated hydration radii for K^+ , NH_4^+ , Na^+ and Ca^{2+} , which are 1.75, 1.88, 2.17 and 2.72 Å, respectively (11). The extremely strong adsorption of DNOC on the clay in the presence of KCl is believed to be mainly due to the interaction between K^+ and the nitro groups on DNOC molecules, but the small hydration radius, and consequent low hydration energy, of K^+ also enables DNOC molecules to easily access the hydrophobic sites at clay surfaces. There is a similar strong adsorption of DNOC in the presence of NH_4Cl for the same reasons, both a possible interaction between NH_4^+ and the nitro groups in the DNOC molecules and access to the clay surfaces. Due to the stronger hydration energies of Ca^{2+} and Na^+ , DNOC adsorption on smectite in both solutions is significantly lower than the other two electrolytes. However, since the hydration energy of Ca^{2+} is higher than Na^+ , the adsorption in the NaCl solution

should be the higher of the two, which is what is found in the literature (7). The opposite result in the current work might be due to the lower concentration of Ca^{2+} .

An XRD spectrum of DNOC adsorption on Swy-2 clay in the presence of NaCl and KCl is shown in **Fig. 4.2 (a)**. It should be noted that the XRD spectrum here reflects the clay d spacing (d_{001}) in the air dried state. In the slurry, due to the swelling of the clay layers, the d spacing would be larger. The peaks on the left side are clay d_{001} peaks in the presence of NaCl with different initial DNOC slurry concentrations, ranging from 0 to 176.3 mg/L from bottom to top. On the right side the peaks are d_{001} peaks in the presence of KCl with different initial DNOC slurry concentrations, from 0 to 172.4 mg/L. In the presence of NaCl, the d_{001} spacing, 15.0 Å, is larger than that in the presence of KCl, 12.0 Å, which is mainly due to the larger hydration radius of Na^+ as mentioned previously. For montmorillonite clay used, the thickness of its silicate layer is about 9.6 Å (12). The thickness of the planar DNOC molecule is estimated to be around 2 Å (13). In the presence of NaCl, the interlayer distance is estimated to be ~5.4 Å, which is large enough to hold the DNOC molecules. In the presence of KCl, this distance is reduced to ~2.4 Å, which is just able to accommodate one layer of DNOC molecules sitting flat and parallel to the clay siloxane surface. Thus, in the presence of KCl, the adsorbed DNOC molecules are much more closely packed at the interlayer. It can also be seen that with the increase of the initial DNOC concentration, there is no significant peak change for either electrolyte, indicating no obvious change in the d_{001} spacing.

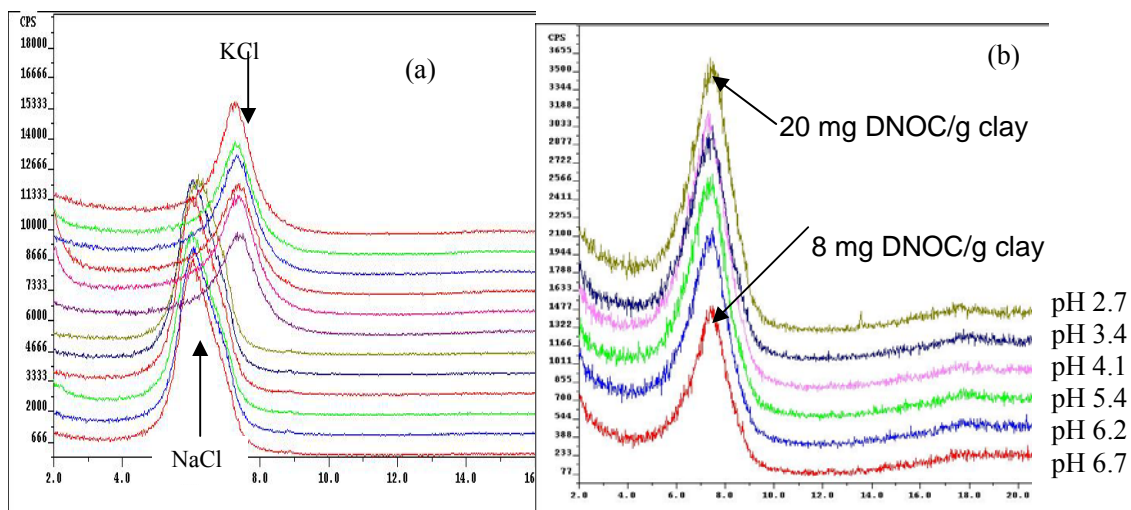


Figure 4.2 (a) XRD spectrum of DNOC adsorption on Swy-2 clay in the presence of NaCl and KCl with different DNOC initial concentrations (for 6 XRD spectra for KCl or NaCl, corresponding from bottom to top to DNOC 0, 8.3, 16.6, 49.8, 83.0 and 166.0 ppm, respectively); (b) XRD spectrum of DNOC adsorption on Swy-2 clay at different pHs in the presence of KCl

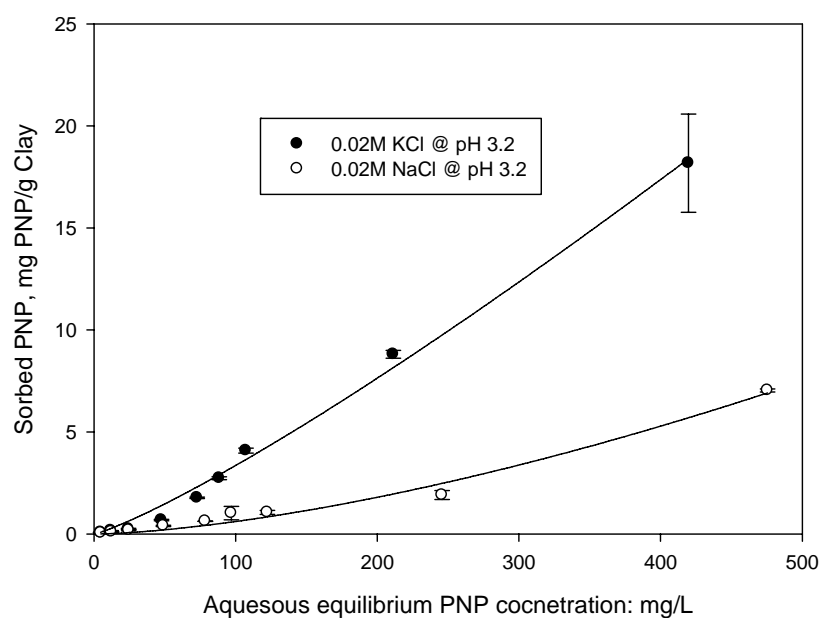


Figure 4.3 Adsorption isotherms of PNP on purified Swy-2 clay

The adsorption of PNP on the purified Swy-2 clay is shown in **Fig. 4.3**. The adsorption isotherms were also fitted with the Freundlich equation, as summarized in Table 1. PNP adsorption on Swy-2 clay is much less than DNOC adsorption. One important reason for this result is the much higher water solubility of PNP (12.4 g/L) than DNOC (198 mg/L). The adsorption of PNP is much greater in the presence of K^+ , in agreement with the DNOC adsorption results. The K_F of the PNP-KCl system (0.0143) is nearly 30 times higher than that of the PNP-NaCl system (0.0005), due to the interaction of K^+ with the nitro group in PNP.

Effect of pH on the adsorption of DNOC

The effect of pH on the adsorption of DNOC in Swy-2 clay slurry is illustrated in **Fig. 4.4**. DNOC is a weak acid with a pK_a of 4.4. In a neutral or basic environment, DNOC exists mainly in its anionic form, while in an acidic environment ($pH < 3.4$), the neutral DNOC molecule is the dominant species. Based on the data shown, the percentage of DNOC being adsorbed on the clay increases sharply with a decrease of pH, indicating that neutral DNOC molecules have a stronger affinity, or less repulsion, to the negatively charged Swy-2 clay surface. In the presence of 0.02M NaCl, sorbed DNOC increased from 1.7% at pH 5.9, to 35% at pH 4.3 and 57% at pH 2.8. Following the same trend but with a larger magnitude, sorbed DNOC in the presence of 0.02M KCl increased from 35% at pH 6.7, to 99.5% at pH 4.1 and 99.7% at pH 2.7, indicating almost complete adsorption when the pH was below the pK_a of DNOC under given experimental conditions. This result for DNOC adsorption on K^+ exchanged Swy-2 clay is in agreement with the literature (14). The XRD spectrum of Swy-2 clay with DNOC adsorption at various pH values is shown in **Fig. 4.2 (b)**. With the decrease of slurry pH, the peak did not shift, though DNOC adsorption on clay

increased from 8.0 to 20.0 mg/g clay, indicating a stable d_{001} spacing of 12.0 Å. It can be inferred that DNOC molecules formed a monolayer at the clay interlayer.

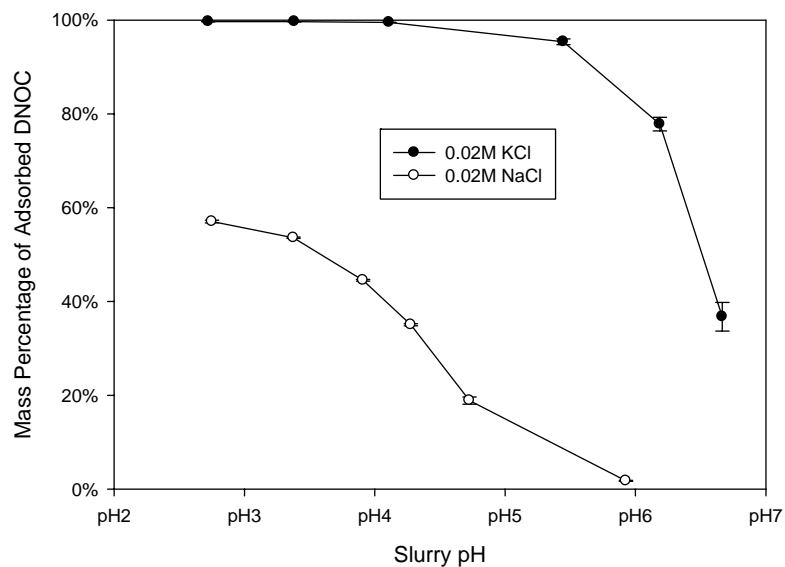


Figure 4.4 DNOC adsorption on purified Swy-2 clay in the presence of KCl or NaCl at different pHs.

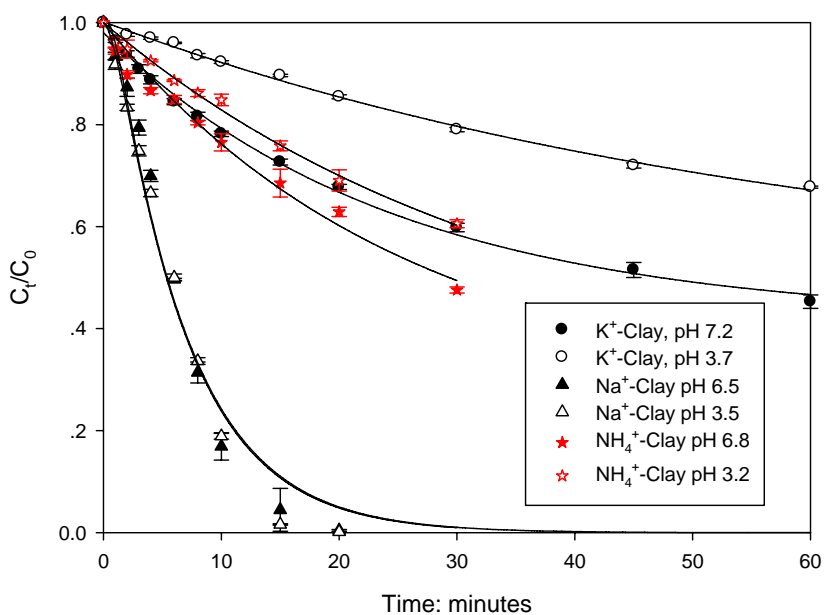


Figure 4.5 Degradation of DNOC by AFT in Swy-2 slurry with different electrolytes and pHs

Degradation of DNOC in Swy-2 slurry by AFT

Degradation of DNOC in purified Swy-2 slurry by AFT was investigated. A 0.50 g sample of purified Swy-2 clay was used to prepare the 100 mL DNOC slurry. Different types of electrolytes, 0.02M KCl, NaCl and NH₄Cl were added. Two slurry pHs, neutral (unadjusted) pH and adjusted low pH, were studied for each type of electrolyte. Degradation results are illustrated in **Fig. 4.5**. The degradation data were fitted with the slurry AFT model (15) with very good fitting ($R^2 > 0.98$). Based on the results, the effect of electrolytes and pH on the degradation rates and kinetics can be discussed.

With the same AFT conditions and electrolyte concentrations, 0.02 M, DNOC degradation rates in the Swy-2 clay slurry follow the order: NaCl >> NH₄Cl > KCl, the opposite order of DNOC affinity on the Swy-2 clay in the presence of the electrolytes, as reported above in the adsorption experiments. Under given experimental conditions, DNOC can be removed completely within 20 minutes in the presence of NaCl, whereas, in the presence of NH₄Cl, there was 50% or more DNOC remaining in the slurry after 30 minutes treatment, depending on the slurry pH. Similarly, in the case of KCl, over 50% DNOC remained in the slurry even after 60 minutes treatment. Based on the adsorption experiments, it was found that DNOC has a weaker affinity for the Swy-2 clay in the presence of NaCl compared with KCl and NH₄Cl. Thus, there is a higher DNOC removal efficiency in the NaCl Swy-2 slurry. On the other hand, the strong affinity of DNOC for Swy-2 clay greatly slows down degradation in the presence of KCl or NH₄Cl.

The pH also affects DNOC degradation rates. In the presence of KCl or NH₄Cl, it was found that DNOC degradation was faster in neutral pH than in low pH. For example, under given experimental conditions, in the presence of 0.02 M KCl, DNOC

removal was ~50% at pH 7.2 after 60 minutes treatment but was 32% at pH 3.7, clearly indicating a low degradation rate at low pH. This finding is opposite to findings in our previous studies (9, 15), where it was found that a low pH enhanced the degradation of probe chemicals either in aqueous solution or soil or clay slurries because of the higher Fenton reaction efficiency at lower pH. The explanation for this contradictory finding relates to adsorption. As reported above, it was found that DNOC adsorption on Swy-2 clay is stronger at lower slurry pH. Under given experimental conditions, DNOC adsorption reached almost 100% at pH 3.7, with minimal DNOC in the aqueous solution. In preliminary studies we used methanol to extract DNOC from the slurry in the presence of KCl. At neutral pH, the extraction efficiency was ~98%; however, the extraction efficiency dropped quickly to <20% at pH 3. Since DNOC has a higher solubility in acetone, we changed the extractant and achieved very good extraction efficiency through all tested pH ranges. This finding clearly demonstrates that DNOC affinity to Swy-2 clay is stronger in the lower pH environment. As a result, DNOC degradation in the presence of KCl was much lower at a lower slurry pH than at a higher pH. The same explanation applies to the NH_4Cl results. But in the case of NaCl, pH has little effect on the DNOC degradation rate. This is the result of two opposite effects. Since the DNOC adsorption is lower overall, the effect of lowered pH, which increases adsorption, and thus decreases degradation, is offset by the Fenton reaction efficiency increase with a decrease of pH, which has a positive effect on degradation.

Through XRD analysis it was found that sorbed DNOC forms a monolayer at the clay interlayer. It should be noted, however, that the XRD sample was air-dried, which was different from the original clay slurry sample. In an air-dried sample, there are limited water molecules at the clay interlayer. In the slurry sample, the clay is soaked with water, which causes the clay to swell, and causes a so-called ‘subaqueous’ phase

to be formed at the clay interlayer. Through computer simulations by other workers (16, 17), it was found that interlayer ‘trapped’ non-cationic organic molecules show a tendency to remain completely in the interlayer aqueous phase. In a companion study (9), it was found through XRD analysis that a probe chemical, mecoprop, was completely removed at the clay interlayer by AFT. It was proposed that Fenton reagents are able to enter the interlayer, where hydroxyl radicals are generated locally. It was verified in that study that the mecoprop desorption process is much slower than the Fenton degradation process. In the current study, the probe chemical DNOC has a much stronger affinity for Swy-2 clay than mecoprop. It is reasonable to infer that the desorption of DNOC from Swy-2 clay is slower than that of mecoprop. Thus the removal of DNOC from the clay interlayer would mainly be due to the degradation reaction with hydroxyl radicals which are generated by the Fenton reagents after entering the clay interlayer subaqueous phase.

Degradation of PNP in clay slurry by AFT

Degradation of PNP in purified Swy-2 slurry by AFT was investigated. A 0.50 g sample of purified Swy-2 clay was used to prepare the 100 mL PNP slurry, and two types of electrolytes, 0.02 M KCl and NaCl, were added. Two slurry pHs, neutral (unadjusted) pH and adjusted low pH, were studied for both electrolytes. The AFT degradation results are illustrated in **Fig. 4.6**. The degradation data were fitted with the slurry AFT model with good fitting ($R^2 > 0.98$). Based on the results, PNP was completely removed from the slurry within 15 minutes under all conditions. When pH was adjusted to 3.2, PNP degradation rates increased in both KCl and NaCl Swy-2 slurry. It is interesting to note that the degradation rate in KCl clay slurry is faster than that in NaCl slurry, though the PNP adsorption in KCl clay slurry is higher, as shown in **Fig. 4.3**.

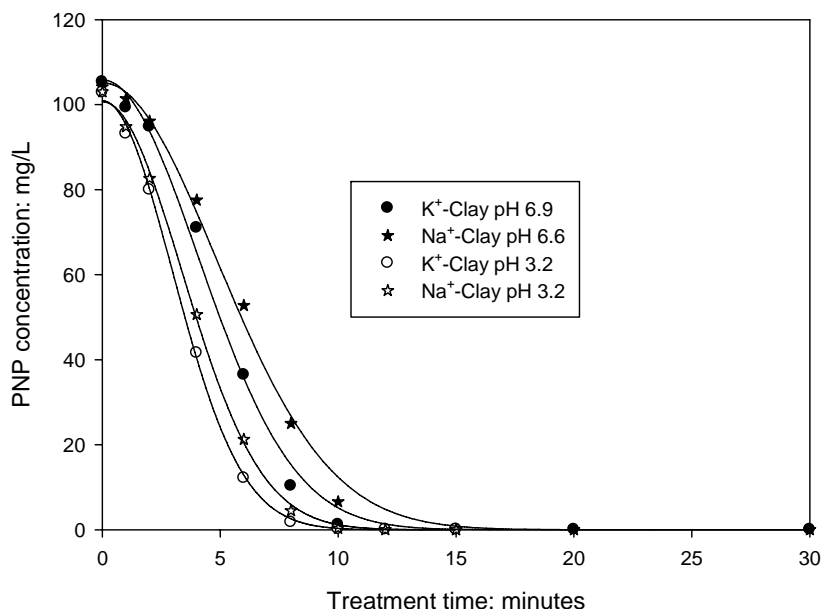


Figure 4.6 Degradation of PNP by AFT in Swy-2 slurry with different electrolytes and pHs

Apparently, the degradation behavior of PNP by AFT is quite different from that of DNOC, especially in the presence of KCl. At least two factors contribute to this difference. First, the much higher water solubility leads to much lower PNP adsorption capacity on the Swy-2 clay, leading to greater degradation. Second, there is only one nitro group in PNP, resulting in a weaker interaction between K^+ and PNP compared to DNOC and less facilitation of adsorption.

DNOC degradation intermediates and pathways

It was found that, due to the interference of the clay, the extraction of DNOC degradation intermediates from the slurry did not provide a sufficient amount for LC-MS or GC-MS analysis. Since it has been documented that the hydroxyl radical is not capable of oxidizing adsorbed organic compounds (18, 19) and the degradation reaction usually takes place in the aqueous phase, it is reasonable to infer that there is

no significant difference between the AFT degradation mechanism of DNOC in aqueous solution or clay slurry.. As a result, instead of studying the degradation intermediates in the clay slurry, DNOC degradation intermediates in aqueous solution were investigated.

A typical HPLC spectrum of possible DNOC degradation intermediates is shown in **Fig. 4.7**. This sample was collected at 7 minutes of AFT treatment, the time shown to have the most peaks based on LC-MS spectral analysis. It was found that DNOC and its degradation intermediates were eluted from the column between 6 and 21 minutes. There were 13 peaks, shown in **Fig. 4.7**, from (a) to (m). Based on the DNOC standard, the peak (l) at 18.65 min was identified as DNOC, also verified by its molecular ion (M^+ , 197). The peak (m) (m/z 367) at 20.45 min, which also was seen in the DNOC standard, was found to be an impurity in the DNOC chemical. The remaining 11 peaks, from (a) to (k) were believed to be DNOC degradation intermediates. The mass spectrum profiles of the 13 peaks are summarized in **Table 4.2**. Except for the peaks (e) at 9.06 and (j) at 12.1 min, the m/z of the molecular ion and the mass spectrum profile for the other 11 peaks are shown in the table.

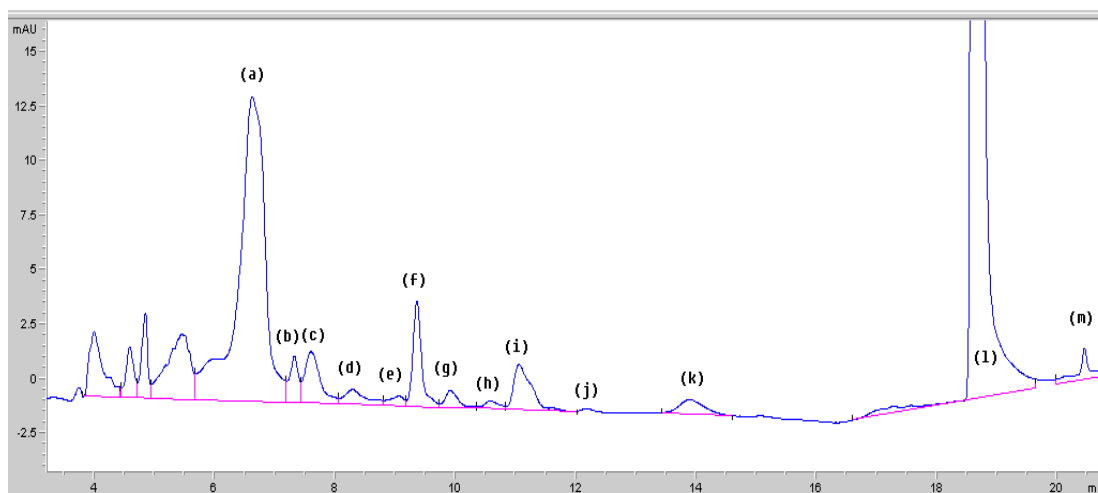


Figure 4.7 An LC spectrum of DNOC degradation intermediates

Table 4.2 Mass spectrum profiles of peaks for DNOC degradation intermediates

Peak	Retention time, min	Molecular ion (M ⁺) m/z	Mass spectrum profile
a	6.62	231	231, 212.9, 182.9, 167.1, 153.1
b	7.32	229	229
c	7.59	245	245.1, 212.9
d	8.28	243	243.1
e	9.06	ND	ND
f	9.35	213	213.0
g	9.91	260	260.0, 197.0
h	10.57	260	260.0, 197.0
i	11.05	211	210.9, 183
j	12.1	ND	ND
k	13.88	227	226.9, 183
l	18.65	197	197, 183 (DNOC)
m	20.45	367	367 (impurity in DNOC)

It is well known that hydroxyl radical reacts with organic compounds, principally by abstracting H from C-H, N-H, or O-H bonds, adding to C=C bonds, or adding to aromatic rings (20). It is believed that Fenton-type oxidation of aromatics mainly occurs with initial formation of a hydroxycyclohexadienyl radical through hydroxyl radical addition, which may be oxidized to a phenol by Fe(III) or undergo a dehydration to a radical cation (21-23). It was found that direct side-chain hydrogen abstraction by the hydroxyl radical is only a minor reaction path with a much slower reaction rate for toluene (21). For the DNOC molecule, there are two available sites for hydroxyl radical attack on the ring and one on the side-chain methyl group. However, due to the strong electron withdrawing effect of the two nitro groups, the

electron density at the two possible attack sites on the ring is decreased, which could depress their reaction rates with strong electrophilic hydroxyl radicals. On the other hand, the side chain reaction rate could be increased. In the AFT system, hydroxyl radicals are generated by freshly delivered ferrous ion (through the electrode reaction: $\text{Fe} \rightarrow \text{Fe}^{2+} + 2\text{e}$) and hydrogen peroxide. Although the delivery of Fenton reagents is different from other Fenton treatment methods, the basic reaction mechanism between hydroxyl radicals and organic molecules is the same for all Fenton methods. Thus, in AFT system, the general reaction mechanisms between hydroxyl radicals and aromatics should apply.

The m/z of the DNOC molecule is 197. One hydroxyl radical addition to the molecule would produce molecules with an m/z of 213. It was found that the m/z of the molecular ion for peak (f) at a retention time of 9.35 min is 213. There are 3 possible products corresponding to an m/z of 213, side-chain reaction product 2-hydroxy-3,5-dinitro-benzyl alcohol, and benzene ring hydroxyl radical addition products 6-methyl-2,4-dinitro-1,5-dihydroxybenzene and 6-methyl-2,4-dinitro-1,3-dihydroxybenzene. We believe that peak f corresponds to benzene ring hydroxyl radical addition products, in accordance with the main reaction scheme mentioned above. A small amount of side-chain reaction product 2-hydroxy-3,5-dinitro-benzyl alcohol is believed to be further oxidized quickly to 2-hydroxy-3,5-dinitro-benzaldehyde, which corresponds to the peak (i) at 11.05 minutes with an m/z of 211. Product (i) can be further oxidized to 2-hydroxy-3,5-dinitro-benzoic acid with an m/z of 227, corresponding to peak (k) at 13.88 minutes. The mass spectrum of peak (k) confirms this assignment: in the spectrum profile, the m/z difference between the molecular ion and the next ion species (m/z 183) is 44, which is the molecular weight of CO_2 . Moreover, this reaction route is also confirmed by the increase of peak (k) and decrease of peak (i) with an increase in AFT treatment time as shown in **Fig. 4.8**.

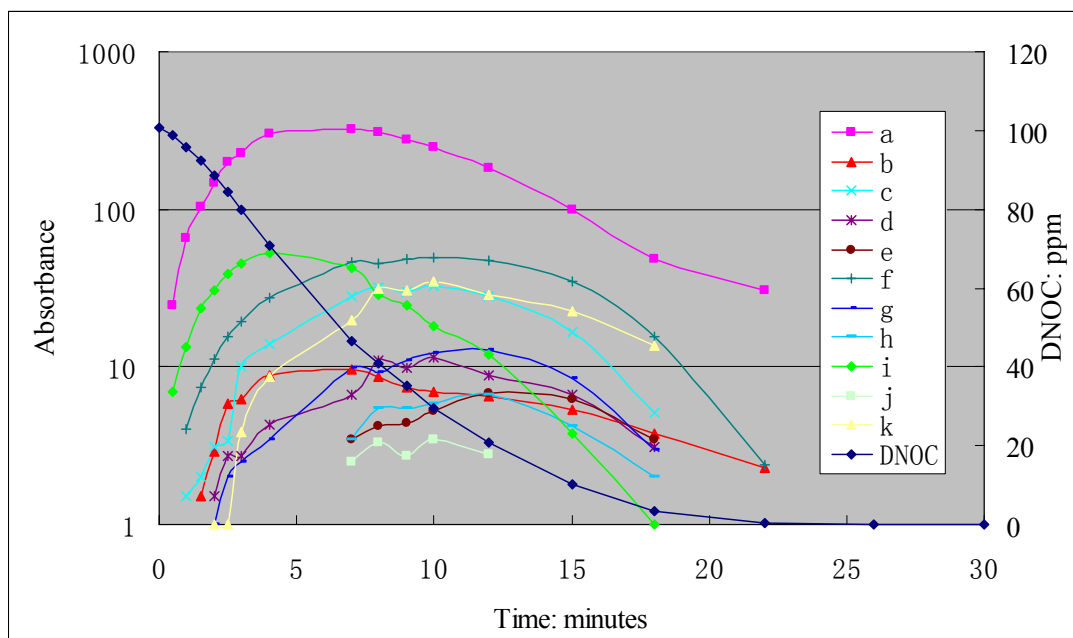


Figure 4.8 Dynamic concentration profiles of DNOC degradation intermediates

The peak (b) at 7.32 minutes with an m/z of 229 should be a compound with two hydroxyl radical additions. There are three possible products, 2,6-dihydroxy-3,5-dinitro-benzyl alcohol, 2,4-dihydroxy-3,5-dinitro-benzyl alcohol, and 2,4-dinitro-6-methyl-1,3,5-trihydroxybenzene. But there is only one peak (b), with an m/z of 229. Based on available information, we cannot assign peak (b) to a specific compound. The peak (c) at 7.59 minutes with an m/z of 245 is assigned as 3,5-dinitro-2,4,6-trihydroxy-benzyl alcohol, a product of three hydroxyl radical additions on the ring and side chain. The peak (d) at 8.28 minutes with an m/z of 243 is assigned as 2,4,6-trihydroxy-3,5-dinitro-benzaldehyde, the product of further oxidation of peak (c). After further oxidation of the side chain, 2,4,6-trihydroxy-3,5-dinitro-benzoic acid is obtained, which corresponds to peak (g) at 9.91 minutes with an m/z of 260. It should be noted that peak (h), with a retention time of 10.57 minutes, also has an m/z of 260. However, this peak did not show up until after 7 minutes treatment. Peak (h) shows

the same mass spectrum as peak (g). As a result, we suspect that the presence of peak (h) is probably due to incomplete separation, and it should be the same product as peak (g). After removal of the carboxyl group from the ring, another hydroxyl radical addition on the ring may occur, resulting in the product 2,4-dinitro-1,3,5,6-tetrahydroxybenzene. We assigned peak (a), the most abundant intermediate, as this product. Based on **Fig. 4.8**, this product was generated from the very beginning of the reaction. However, because all available sites on the benzene ring have been occupied by two nitro groups and four hydroxyl groups, the rates of further reactions between hydroxyl radicals and this intermediate, such as ring cleavage or substitution of nitro groups, should be much slower than the preceding reactions. Therefore, this intermediate accumulates and becomes the most abundant product during the treatment.

In order to investigate whether nitro groups have been cleaved from the ring, the inorganic nitrogen concentration in $\text{NO}_3^-/\text{NO}_2^-$ and NH_4^+ were monitored, as shown in **Fig. 4.9**. It can be seen that $\text{NO}_3^-/\text{NO}_2^-$ -N concentration (mg/L) in the reaction cell increased quickly from the beginning of the treatment until 10 minutes into it. Then this concentration decreased quickly with further treatment. This finding clearly shows that nitro groups on DNOC molecules have been removed during the reaction. Based on the calculation, initial total nitrogen concentration in the reaction cell was about 14 mg/L, all in the organic form. At 10 minutes the total inorganic nitrogen concentration was about 4.0 mg/L, around 29% of the initial total nitrogen content. It is interesting to note a decrease in inorganic nitrogen concentration after 10 minutes treatment, which was not observed by others (24). In the AFT system, with the increase in treatment time, the pH of the reaction slurry or solution drops. It was found in the present study that the pH dropped to ~pH 3 after 5 minutes treatment. It is well known that NO_3^- has a strong oxidizing capability in an acidic environment. With the presence of the iron

plate in the slurry (as the anode), the much diluted nitric acid reacts with iron, and NO_3^- would be reduced to NO gas or ammonium ion, NH_4^+ . We conclude that the loss of inorganic nitrogen in the system is due to the escape of NO gas from the system.

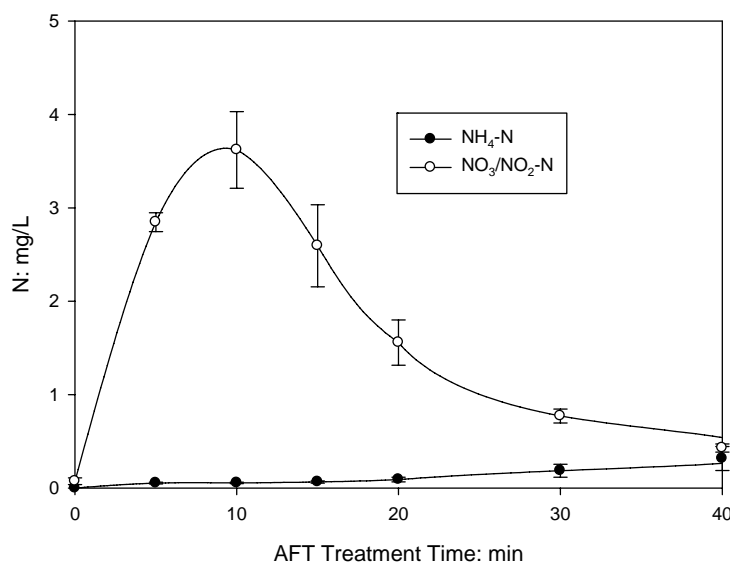
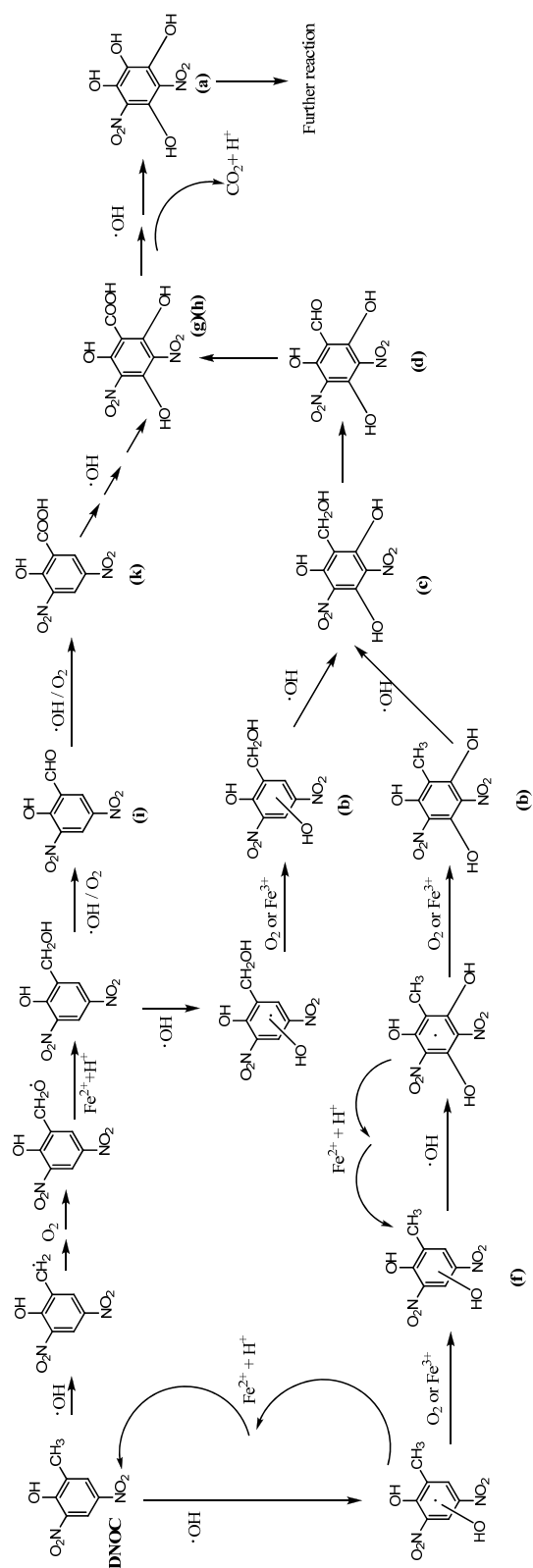


Figure 4.9 Inorganic nitrogen concentration profile during the AFT treatment

The concentration of $\text{NH}_4^+\text{-N}$ increased slowly during the treatment, with the highest concentration at ~ 0.3 mg/L. In other work, the authors proposed that the origin of NH_4^+ in a TiO_2 photo catalytic degradation system was from the reduction of nitro groups on DNOC molecules (24). However, due to the presence of hydrogen peroxide, the environment in the AFT system is highly oxidizing. Thus, we do not expect reduction of nitro groups on the DNOC molecule. We propose that the ammonium is generated from the reduction of nitrates by iron as mentioned above.

Based on the above analysis, a DNOC degradation pathway in the AFT system is proposed, as shown in **Scheme 4.1**. It should be noted that this scheme shows only some reaction steps at the beginning of the degradation process, based on available LC-MS data. It is proposed that there are two reaction routes. One is hydroxyl radical

reaction with the side-chain methyl group. First, one hydrogen is abstracted from the methyl group by the hydroxyl radical, producing an organic radical. In the presence of oxygen in the aqueous solution, this radical will react with oxygen, producing peroxy radicals or oxyl radicals as shown in the Scheme 1. These radicals may then react with ferrous ions in the solution, with the production of alcohol. In this oxidizing environment, the alcohol can be further oxidized to aldehyde and carboxylic acid. The other reaction route is hydroxyl radical addition on the benzene ring, producing an important intermediate product, 2,4-dinitro-1,3,5,6-tetrahydroxybenzene (m/z 231). As shown in Scheme 1, a hydroxycyclohexadienyl radical is formed after the addition of one hydroxyl radical. In the presence of oxygen and ferric ion, phenolic products are generated quickly from the radical; meanwhile the radical could also react with ferrous ion at a much lower rate and reform the parent compound. With the releasing of carbon dioxide, after the carboxylic group is cleaved from the ring, 2,4-dinitro-1,3,5,6-tetrahydroxybenzene is generated. Since there is no site on the benzene ring available for hydroxyl radical addition or oxidation, this product is relatively stable and its accumulative concentration is high. Based on the nitrogen measurement, nitro groups on the benzene ring have been removed, either due to hydroxyl radical substitution or benzene ring cleavage. Unfortunately, no ring cleavage product has been detected under our analysis conditions.



Scheme 4.1 Proposed DNOC degradation pathways

4.4 Conclusions

The adsorption and degradation of two nitro aromatic compounds, DNOC and PNP in Swy-2 clay slurry were investigated. It was found that the adsorption behavior of DNOC directly relates to the types of electrolytes and slurry acidity. In the presence of KCl or NH_4Cl , DNOC has a strong affinity to the clay due to complex formation between these cations and DNOC molecules; however, in the presence of NaCl or CaCl_2 , the adsorption capacity was much less. It was also found that DNOC adsorption is favored in an acidic environment, and at given experimental conditions, DNOC molecules can be completely adsorbed on the clay surface at pH values below the pK_a (pH 4.4). It was inferred that adsorbed DNOC forms a monolayer at the clay interlayer based on XRD analysis. PNP adsorption was also favored in the presence of KCl compared with NaCl.

Through AFT experiments, we conclude that DNOC and PNP can be removed from the clay interlayer, though the degradation rate decreased with an increase of slurry acidity. This result offers an important implication for remediating NAC contaminated soils: choosing appropriate pH is critical to achieve the remediation goal. Based on the LC-MS data, 9 possible degradation intermediates have been detected and assigned, and a possible degradation pathway has been proposed. Based on the nitrogen measurement, we conclude that nitro groups have been removed from the benzene rings and DNOC molecules have been mineralized during the AFT process.

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Chapter 5

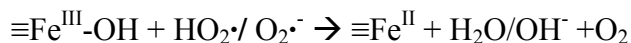
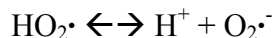
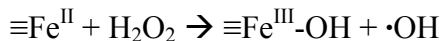
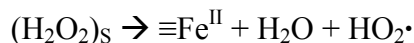
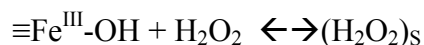
Effect of Goethite on the Degradation of Dinoseb by AFT

5.1 Introduction

The Fenton reaction based oxidation treatment method, one of the most often used advanced oxidation processes, has been widely studied as a method to remove organic pollutants in both water and soil slurry systems. Fenton-based membrane anodic Fenton treatment (AFT), developed in our laboratory (1), employs ferrous ion freshly generated by the electrochemical reaction ($\text{Fe} \rightarrow \text{Fe}^{2+} + 2\text{e}^-$) and hydrogen peroxide pumped continuously into the reactor.

In previous studies (2, 3) the effect of humic acid and clays, including kaolinite and montmorillonite clay, on the AFT degradation of selected organic agrochemicals in slurry systems was measured. It was found that both the degradation rate and efficiency were negatively affected by the adsorption or pH buffering of humic acid or clay, and a kinetic model was developed to describe the degradation in a slurry system.

In addition to clays, it is believed that other soil minerals, such as iron oxides, also affect the AFT degradation of organic pollutants because of their reaction with hydrogen peroxide and their potential adsorption capacity. Watts et al. (4, 5) found that iron minerals could be used to remove organic contaminants from soil in the presence of hydrogen peroxide. Lin et al. (6) explored the reaction mechanism between goethite and hydrogen peroxide. They proposed that goethite acts as a catalyst in the decomposition of hydrogen peroxide; a simplified reaction mechanism was summarized as following:



In the above proposed reaction steps, $\equiv\text{Fe}^{\text{III}}\text{-OH}$ represents the goethite surface; $(\text{H}_2\text{O}_2)_\text{s}$ represents the surface hydrogen peroxide after forming a precursor complex with the goethite surface; $\equiv\text{Fe}^{\text{II}}$ represents the goethite surface iron reduced by hydrogen peroxide. On the basis of the above reaction steps, it can be seen that hydroxyl radical is generated during the decomposition of hydrogen peroxide catalyzed by goethite. In addition, there is some dissolution of iron oxides in the water solution, producing a limited amount of free ferric ions, which will react with hydrogen peroxide producing ferrous ions. As a result, in the presence of hydrogen peroxide and iron oxides, hydroxyl radicals and other oxygen containing radicals can be produced, and these radicals are then able to react with organics if available.

In the present study goethite was selected as a representative of iron oxides. Goethite is the most common and the most thermodynamically stable iron oxide in soils. It has double bands of $\text{FeO}(\text{OH})$ octahedra sharing edges and corners with hydrogen bonding between the bands (7). Dinoseb ($\text{pK}_\text{a}=4.7$) was selected as a probe chemical. Its chemical structure and some of its physical/chemical properties can be found in **Table 1.1**. The use of dinoseb was cancelled in the U.S. in 1986 due to its potential risk of birth defects and other adverse health effects for applicators and other persons with substantial dinoseb exposure (8). However, it is still allowed for use in many other countries, such as China and India.

The objectives of this study are: (1) to investigate the effect of goethite on the AFT degradation of dinoseb and (2) to investigate the effect of pH and goethite content on the degradation of dinoseb.

5.2 Materials and Experiments

Chemicals

Granular goethite, dinoseb (99%) and hydrogen peroxide (30%, analytical grade) were purchased from Sigma-Aldrich (St. Louis, MO). Water and acetonitrile, both HPLC grade, were purchased from Fisher Scientific (Pittsburgh, PA). Deionized water (electricity resistant, $R \geq 18.1 \text{ M}\Omega \cdot \text{cm}^{-1}$) was produced by an MP-1 Mega-PureTM system (Corning, NY)

Adsorption experiments

Adsorption batch experiments were conducted to obtain adsorption isotherms for dinoseb in the goethite slurry. Based on a preliminary adsorption kinetics study (data not shown), the adsorption equilibrium can be attained within 24 hours. 20.0 mg goethite and 20.0 mL dinoseb solutions were placed in 25 mL glass vials; pH was adjusted by 0.01 M HCl if needed. After 24 h shaking, a 1.0 mL sample was collected, and after 20 min-centrifuging at 10,000 rpm, the supernatant was collected for concentration analysis. The amount of adsorbed dinoseb was calculated based on the difference in aqueous concentration between the initial time and 24 h.

AFT batch experiments

All experiments were carried out in two 150-mL glass cells; a scheme of the experimental apparatus is shown in Fig. 1.1. Detailed descriptions of the AFT process can be found in the literature (2, 3). 100.0 mL of dinoseb and goethite (1.0 g/L) slurry with 0.02M NaCl was added to the anodic half-cell, and the same volume of 0.08M

NaCl solution was added to the cathodic half-cell. The electrolysis current was controlled at 0.050 A. Hydrogen peroxide solution (0.311 M) was delivered to the anodic half-cell at a rate of 0.50 mL min⁻¹. Goethite concentration and molar ratio of H₂O₂ and Fe²⁺ were kept at 1 g/L and 10:1, respectively, unless specified. At given time intervals, a 0.7 mL sample was collected and added to a 1.5 mL tube containing 0.7 mL methanol which was used to quench hydroxyl radicals and to extract probe chemicals from the slurry in order to get the total concentration. The methanol extraction efficiency of dinoseb extraction was greater than 99%. Two control experiments were conducted to investigate the dinoseb loss in the goethite slurry in the presence of Fe²⁺ or H₂O₂ alone. The experiments were repeated twice.

Concentration measurement

The concentration of dinoseb samples was measured by an Agilent 1200 HPLC equipped with a diode array detector (Agilent Technologies, Inc, Santa Clara, CA). The mobile phase was composed of 80% acetonitrile and 20% HPLC grade water with 1% acetic acid. A carbon eighteen 5 µm 150 mm × 4.6 mm (i.d.) Agilent reverse phase column was used. Flow rate was set to 1.0 mL/min. The chosen UV wavelength for dinoseb was 268 nm. The concentration of total iron in the solution was obtained based on the 1,10-phenanthroline method.

5.3 Results

Dinoseb adsorption on goethite

The adsorption isotherm of dinoseb on goethite particles is shown in **Fig. 5.1 (a)**. The concentration of goethite was 1.0 g/L, and the slurry pH values were not adjusted. It can be seen that with the increase of dinoseb concentration in the goethite slurry, dinoseb adsorption capacity on the goethite increases. This is probably due to the lower pH of the slurry with the higher concentration of dinoseb, a weak acid with a

pKa of 4.7. The pH values of slurry with 1.34 and 26.7 mg/L dinoseb were 5.73 and 4.80, respectively, indicating that adsorption of neutral dinoseb molecules was favored. The effect of pH on adsorption is further illustrated in **Fig. 5.1 (b)**. For the same initial dinoseb concentration, when pH was unadjusted (6.5), only ~10% of dinoseb was adsorbed on the goethite. However, when the pH was adjusted to 2.9, the adsorbed dinoseb increased to nearly 40%, clearly demonstrating that dinoseb adsorption is favored in an acidic environment.

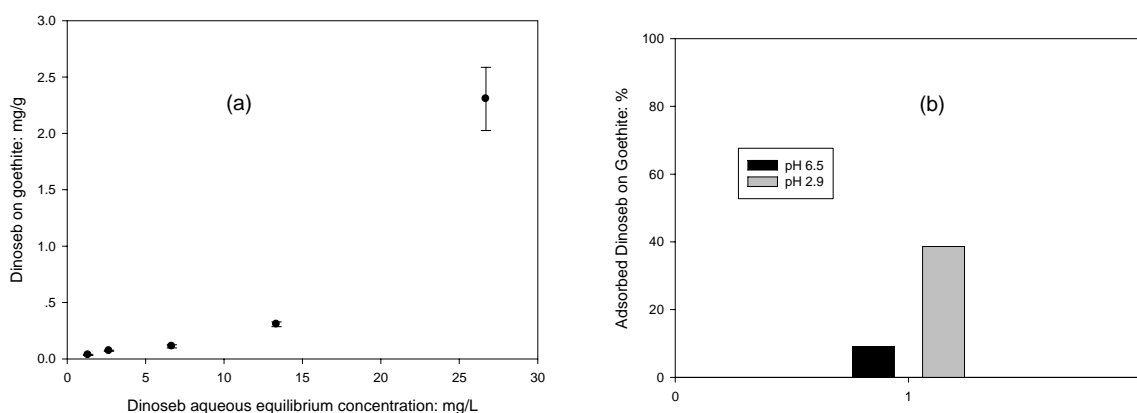


Figure 5.1 (a) Dinoseb adsorption isotherm in goethite slurry; (b) Effect of slurry pH on the dinoseb adsorption

Dinoseb degradation by AFT

(1) Dinoseb degradation in aqueous solution

The degradation of dinoseb by AFT in aqueous solution was investigated, and the results are shown in **Fig. 5.2**. Two control experiments were also conducted to investigate the dinoseb loss in the presence of Fe^{2+} or H_2O_2 alone, and the data are shown in the figure. On the basis of the results, in the presence of H_2O_2 alone more than 92% of the initial total dinoseb remained in the solution; while in the presence of Fe^{2+} alone, there was nearly 21% dinoseb loss after 30 minutes. Though the exact

cause of dinoseb loss in the presence of Fe^{2+} was not clear, it could be related to the generation of ferrous ions which were produced through the electrode reaction. It can be seen that dinoseb was completely removed by AFT in 5 minutes, clearly demonstrating the effectiveness of AFT. The degradation curve was well fitted with the classic AFT model as mentioned in the Chapter 1.

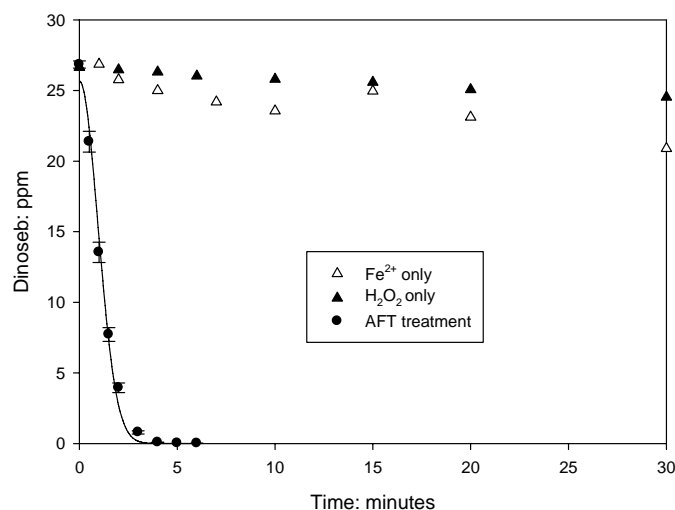


Figure 5.2 AFT degradation of dinoseb in aqueous solution

(2) Dinoseb degradation in goethite slurry

Degradation of dinoseb in 1.0 g/L goethite slurry is shown in **Fig. 5.3**. All initial slurry pH values were neutral or unadjusted. Two control experiments were also conducted in the presence of Fe^{2+} or H_2O_2 alone. Based on the results, in the presence of H_2O_2 , more than 93% of initial total dinoseb remained in the slurry; while in the presence of Fe^{2+} alone, there was more than 19% dinoseb loss after 30 minutes. This result is very similar to the result obtained in aqueous solution, clearly indicating that, under the given experimental conditions, dinoseb loss due to the presence of goethite is negligible. Similarly, dinoseb in the slurry could be completely degraded in 5

minutes, with a very good fit to the slurry AFT model (solid line). The model equation is shown below; detailed model development was documented elsewhere (3).

$$[P]_t = ([P]_0 - \delta)e^{-k_{P,OH}[OH]_{SS}[t-(1-e^{-\lambda t})/\lambda]} + \delta$$

$[P]_0$ and $[P]_t$ are dinoseb concentrations (ppm or μM) at $t=0$ and t , respectively; δ is the residue dinoseb concentration (ppm or μM) that is not available for degradation; $k_{P,OH}$ is the reaction rate constant between dinoseb and hydroxyl radical ($\text{min}/\mu\text{M}$); $[OH]_{SS}$ is the steady state hydroxyl radical concentration (μM); and λ is a coefficient related to the production and consumption of hydroxyl radical (min^{-1}).

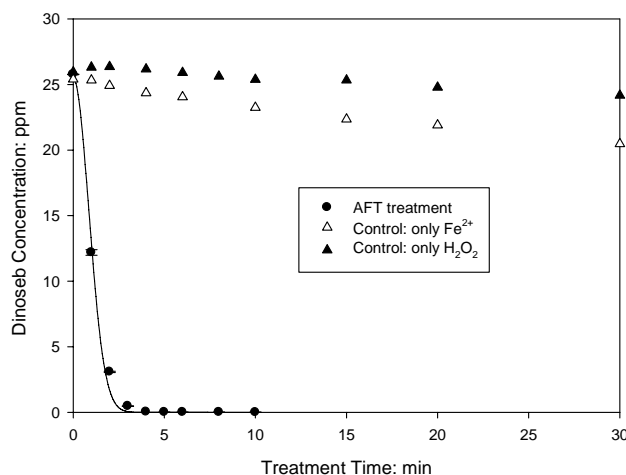


Figure 5.3 AFT degradation of dinoseb in 1.0 g/L goethite slurry

(3) Effect of goethite content on dinoseb degradation

The slurry goethite content was varied and the dinoseb degradation results are shown in **Fig. 5.4 (a)**. The slurry pH values were not adjusted. It can be seen that, with an increase of goethite content in the slurry from 0 g/L to 5.0 g/L, the degradation curves do not shift significantly, and they almost overlap with one another. The initial equilibrium aqueous dinoseb concentrations in the goethite slurry were measured, and it was found that these slurries had very similar equilibrium aqueous dinoseb

concentrations, indicating that dinoseb adsorption on the goethite surface did not change significantly with an increase of goethite content in the slurry. This finding showed that, under the given experimental conditions, adsorption did not affect the degradation of dinoseb by AFT.

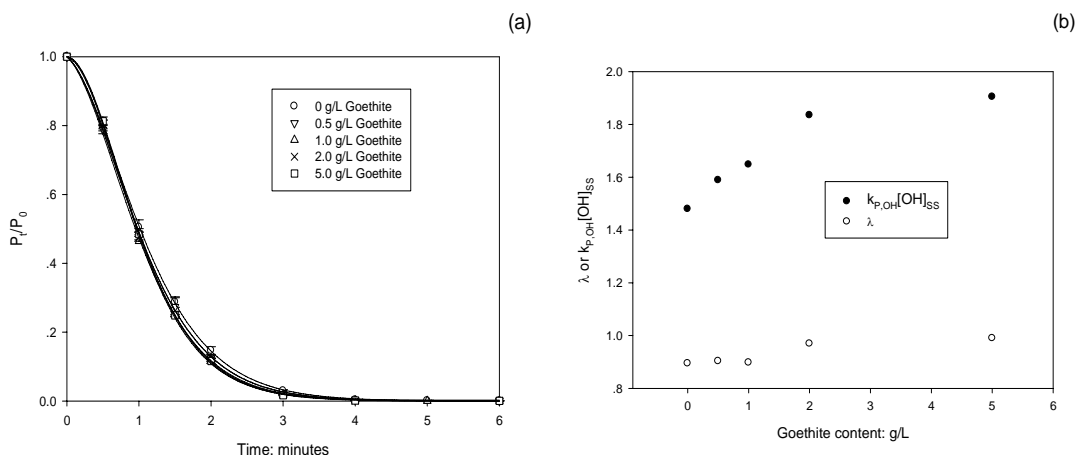


Figure 5.4 (a) Effect of goethite content on the AFT degradation of dinoseb; (b) slurry AFT model fitting parameters

The slurry AFT model fitting parameters, $k_{P,OH} [OH]_{SS}$ and λ are shown in **Fig. 5.4 (b)**. Due to the complete removal of dinoseb, the values of the fitting parameter δ for tested goethite slurries were all very small, and they are not shown in the figure. Based on the figure, with the increase of goethite content from 0 to 5.0 g/L, $k_{P,OH} [OH]_{SS}$ increases from 1.48 to 1.90. Since all experiments were conducted at the same room temperature, the values of the reaction rate constant, $k_{P,OH}$, should be the same for all tested slurries. The change of the fitting parameter $k_{P,OH} [OH]_{SS}$ reflects a change in the $[OH]_{SS}$, steady state concentration of the hydroxyl radical. It can be inferred that $[OH]_{SS}$ increases with an increase of goethite content, indicating higher dinoseb degradation efficiency in the slurry with a higher goethite content. There are two possible reasons for this result. The first one is the higher hydrogen peroxide

decomposition rate due to higher content of goethite. Lin et al. (6) found that the hydrogen peroxide decomposition rate was proportional to the goethite content in a slurry. As a result, there was more hydroxyl radical produced through the mechanisms mentioned in the Introduction. Another important reason is related to the soluble iron concentration in the goethite slurry. Based on the total iron measurements, it was found that under neutral conditions, there was 0.5-0.6 mg/L soluble iron in the aqueous phase of 1.0 g/L goethite slurry. This additional soluble iron would be able to enhance the Fenton reaction in the AFT system, resulting in more generated hydroxyl radicals. For a higher content of goethite, there should be a higher concentration of soluble iron species in the slurry. This also explains the increase of $[OH]_{ss}$ with an increase of goethite content.

In the slurry AFT model, λ governs the time needed for the hydroxyl radical to reach the steady state. Based on **Fig. 5.4(b)**, λ increased slightly with an increase of goethite content in the slurry, indicating less time needed to reach a steady state for the hydroxyl radical.

(4) Effect of pH on the AFT degradation of dinoseb

The initial goethite slurry was adjusted to pH 2.9, and the effect of pH on the dinoseb degradation was studied. The results are shown in **Fig. 5.5**. Two control experiments on the loss of dinoseb in the presence of H_2O_2 alone were also conducted at both high and low pH values. At high pH, dinoseb loss during 30 minutes was ~ 7%. However, at pH 2.9, the dinoseb loss was ~50%. This 50% loss is believed to be due mainly to the attack of hydroxyl radicals produced by a Fenton reaction between the soluble iron species and hydrogen peroxide. The soluble iron concentrations at both high and low pH were measured and the results are shown in **Table 5.1**. The soluble

iron concentration at low slurry pH, is 5 to 6 times higher than that at high pH, which explains the greater dinoseb loss at low pH in the presence of hydrogen peroxide.

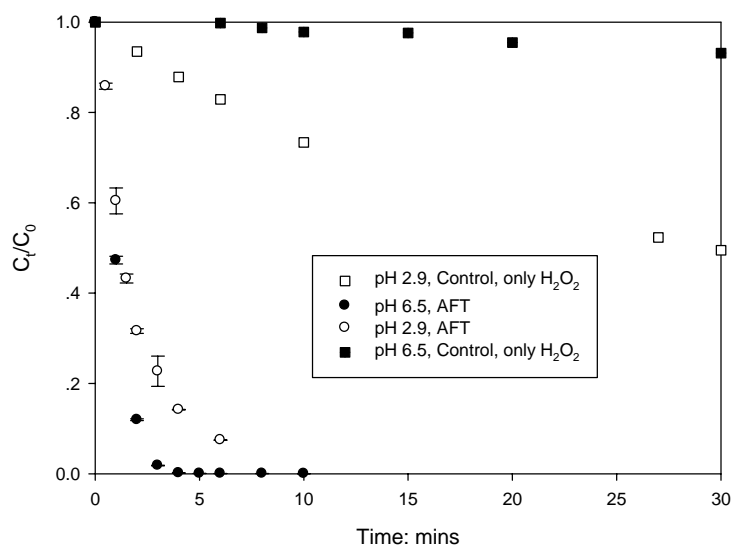


Figure 5.5 Effect of pH on the AFT degradation of dinoseb

Table 5.1 Soluble iron concentration in 1.0 g/L goethite slurry

pH	Total Fe: mg/L
pH 6.5 unadjusted	0.51
pH 6.5 unadjusted	0.64
pH 3	3.10
pH 3	3.10

Dinoseb degradation at high and low slurry pH is also shown in **Fig. 5.5**. Surprisingly, it was found that the dinoseb degradation rate decreased at low slurry pH. For the slurry with an initial pH of 6.5, dinoseb was completely removed in 5 minutes. However, for the slurry with an initial pH of 2.9, there was still ~ 7.4% dinoseb

remaining in the slurry after 6 minutes of AFT treatment. This result was opposite from our previous research results for synthetic soil or montmorillonite clay slurries, where it was found that the degradation of carbaryl and mecoprop was enhanced by decreasing the slurry pH values (2, 3). However, this result was in accordance with our previous research results for the degradation of 4,6-o-dinitrocresol in montmorillonite clay slurry. Similarly, it was believed that the cause for the lower degradation rate was due to the greater adsorption at the lower pH. As discussed in the adsorption experimental results, with the adjustment of pH from 6.5 to 2.9, sorbed dinoseb on goethite particles increased significantly from 10% to 40%, which slowed the degradation that took place mainly in the aqueous phase of the slurry.

In this study the effect of goethite on the AFT degradation of dinoseb was investigated. It was found that pH plays an important role in the adsorption and degradation processes. At neutral or high pH, there was less dinoseb adsorption on goethite, and the AFT degradation process was not significantly affected under the given experimental conditions. In an acidic or low pH environment, there was much greater dinoseb adsorption on goethite than at higher pH, and the AFT degradation process was inhibited by the adsorption, though there was more soluble iron originating from the goethite that could enhance the degradation. Through model fitting parameter analysis, it was found that a higher goethite content could increase the degradation efficiency due to more soluble iron species in the slurry. It was also found that goethite itself could remove 50% of dinoseb in the presence of hydrogen peroxide in 30 minutes in an acidic environment, providing important implications for the application of hydrogen peroxide in iron rich soil remediation.

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Chapter 6

Conclusions

This thesis investigated the application of anodic Fenton treatment to the degradation of several probe agrochemicals in model soil slurry systems. A kinetic model, called the slurry AFT model, was developed to describe the degradation process in the slurry system. Effects of different model soil components, such as humic acid, kaolin or montmorillonite clay, and goethite, on the degradation of different groups of agrochemicals, including carbaryl, mecoprop, paraquat, 4,6-o-dinitrocresol, p-nitrophenol and dinoseb were studied. The main results and conclusions are summarized in the following sections. The environmental implications of this study and directions for future research were also discussed at the end of this chapter.

6.1 Summary of the main results

In Chapter 2, a synthetic soil, which is a mixture of humic acid, sand and kaolinite clay, was used in the slurry system. AFT degradation of a widely used pesticide, carbaryl, in the synthetic soil slurry was investigated, and the following primary results were obtained.

- (1) An empirical slurry AFT model was developed to describe the organic chemical degradation process in the slurry system. Three important assumptions were made during the kinetic model development process. One was the steady state approximation for hydroxyl radical, and the second one was the assumption that the degradation reaction between hydroxyl radical and target organic chemical took place in the aqueous phase of the slurry. The

third assumption is the definition of a loosely defined constant that relates to the strongly adsorbed or non-labile pesticide that is not available for degradation within the time frame of AFT treatment. The model equation had a very good fit with the experimental data.

- (2) The effect of humic acid content, initial slurry pH, initial carbaryl concentration, Fenton reagent delivery ratio, and soil/water ratio (w/v) on the degradation rate was also investigated. It was found that: with an increase of 0 to 2.5% humic acid content in the artificial soil, the carbaryl degradation rate slowed down greatly; when the initial slurry pH was adjusted to a lower value, the carbaryl degradation rate increased compared to that in slurries with an unadjusted initial pH of 5.5; the initial carbaryl concentration did not affect the degradation rate, but the slurry with higher initial carbaryl concentration had a higher carbaryl residual concentration; under the given experimental conditions, a 2:1 $\text{H}_2\text{O}_2/\text{Fe}^{2+}$ ratio was preferred from the perspective of cost effectiveness; and the degradation rate decreases significantly in a slurry with a lower soil/water (w/v) ratio.
- (3) The experimental data were fitted with the model equation, and all three fitting parameters, $k_{P,OH}[\cdot OH]_{SS}$, λ , and δ (or δ/P_0 for the normalized model equation) were summarized and interpreted.

In Chapter 3, a 2:1 layered clay, Swy-2 montmorillonite, was used in the slurry system, and three widely used organic agrochemicals, carbaryl, mecoprop and paraquat were selected as probe chemicals. The AFT degradation of these chemicals in the clay slurry system was studied, and the effects of different adsorption mechanisms on the degradation were investigated and discussed. The main results are summarized below.

- (1) Adsorption isotherms were obtained for all three chemicals: mecoprop and carbaryl have curves fitted with the Freundlich equation, and paraquat has a curve fitted with the Langmuir equation. Through measuring the d spacing of the clay layer before and after adsorption, molecular disposition at the clay interlayer was inferred: both mecoprop and paraquat appear to form a monolayer sitting flat and parallel to the clay siloxane surfaces.
- (2) Through AFT degradation experiments, it was found that carbaryl and mecoprop could be completely and quickly removed from the slurry, while for paraquat, only the chemical in the aqueous phase of the slurry could be degraded.
- (3) Through XRD analysis, it was found that the AFT degradation rate of interlayer adsorbed mecoprop was much higher than the desorption rate, indicating that AFT is capable of effectively degrading interlayer adsorbed mecoprop. However, due to lack of interlayer water and reduced interlayer distance, strong and tight adsorption of paraquat at the clay interlayer protects paraquat from being attacked by hydroxyl radicals.

In Chapter 4, Swy-2 montmorillonite clay was used in the slurry system, and the adsorption and degradation of 4, 6-*o*-dinitrocresol (DNOC) and *p*-nitrophenol (PNP) in the clay slurry were investigated. The main results are summarized below.

- (1) The pH and type of cations were varied, and results showed that adsorption of DNOC and PNP increased at lower pH values. The specific cation had a significant effect on adsorption, which was dramatically enhanced in the presence of K^+ and NH_4^+ . Nitroaromatic compounds adsorb on the montmorillonite clay through the formation of complexes between the clay interlayer certain cations, such as K^+ or NH_4^+ , and the nitro groups on the

molecule. Moreover, DNOC adsorption is favored in an acidic environment, and DNOC molecules can be completely adsorbed on the clay surface at pH values below the pKa (pH 4.4).

- (2) DNOC degradation rates were affected by the initial pH and the type of electrolytes. The degradation rate substantially decreased in the clay slurry system in the presence of K^+ and low pH, with a large amount of DNOC residue remaining after 60 min treatment.
- (3) Based on the LC-MS data, 9 possible degradation intermediates were detected and assigned, and a possible degradation pathway was proposed. Based on the nitrogen measurement, it was found that nitro groups were removed from the benzene rings and DNOC molecules were mineralized during the AFT process.

In Chapter 5, a widely distributed iron oxide, goethite, was used in the slurry system, and dinoseb was selected as the probe chemical. The effect of goethite on the AFT degradation of dinoseb was investigated. Major results are summarized below.

- (1) pH effect on the adsorption and AFT degradation of dinoseb in the goethite slurry was investigated. At neutral or high pH, there was less dinoseb adsorption on goethite than at low pH, and the AFT degradation process was not significantly affected under the given experimental conditions. In an acidic or low pH environment, there was much more dinoseb adsorption on goethite, which inhibited AFT degradation, though more soluble iron originated from goethite in acidic conditions, a potential enhancement for degradation. We also found that goethite itself could remove 50% dinoseb in the presence of hydrogen peroxide in 30 minutes in an acidic environment.

- (2) Through model fitting parameter analysis, it was found that higher goethite content could increase the degradation efficiency due to more soluble iron species in the slurry.

6.2 General conclusions and environmental implications

Based on the results of studies of AFT degradation of several organic agrochemicals in slurry systems, we conclude that:

- (1) The developed slurry AFT model is well able to describe the degradation of non-cationic organic chemicals in a slurry system.
- (2) AFT is an effective method to remove non-cationic organic chemicals in soil or clay slurry systems. AFT is capable of effectively degrading interlayer non-cationic organic chemicals that are usually not available for biodegradation.
- (3) Adsorption of organic chemicals by soil organic matter, clay or oxides may affect the degradation process differently depending on the nature of the organic chemicals and the adsorption mechanisms. Except for nitroaromatic compounds, which have distinct adsorption mechanisms on smectite clay, for most other neutral or anionic organic pollutants, their adsorption on SOM generally outweighs their adsorption on clays or other oxides, and SOM is a more important factor to study the fate and transport of organic pollutants in soil. For cationic organic chemicals, their adsorption on clay will be more important, especially in soils with a large content of layered clays with high CEC since they cannot be removed effectively by AFT at the clay interlayer.
- (4) Through AFT experiments, we conclude that nitroaromatics, DNOC and PNP can be removed from the montmorillonite clay interlayer, though the

degradation rate decreased with an increase of slurry acidity or the presence of certain cations. This result offers an important implication for remediating NAC contaminated soils: choosing appropriate pH is critical to achieve the remediation goal.

- (5) Generally speaking, though the adsorption effect in an acidic environment is notable, iron oxides do not affect the AFT degradation of organic chemicals in the slurry system significantly due to the high aggressiveness and efficiency of AFT.

In summary, The Fenton reaction-based AFT process is capable of removing neutral or anionic organic chemicals adsorbed at the clay interlayer effectively, which is an advantage over bioremediation methods in these systems. The AFT method is an effective and reliable option for treatment, on a small scale, of soils that are highly contaminated by organic pollutants. The findings from adsorption experiments and XRD results for different types of organic agrochemicals may benefit our understanding of their fate and transformation in soils. The findings also have important implications for selecting soil remediation strategies.